

KULAKARNI CONSULTANTS
STRUCTURAL ENGINEERS, PROJECT CONSULTANTS & ARCHITECTS


STRUCTURAL STABILITY CERTIFICATE

This is to certify that the structural designs/drawings of Amenities Block consisting Stilt plus Four upper floors in the proposed gated community lay-out cum group housing in Sy. No. 786 (P) situated at Miryalaguda Town and Mandal, Nalgonda District, Telangana belonging to Mrs. A. Vasudha Reddy & others all are residents of Flat No. A-402, Aditya Hill Top, Road No. 82, Jubilee Hills, Filmnagar Sub-port, Hyderabad are prepared by us. We are the structural consultants for the above said proposed residential gated community group housing lay-out.

The designs and drawings of RCC framed structure pertaining to the proposed Amenities Block shall confirm to the National Building Code of India relevant I.S Code's of practice for design and construction.

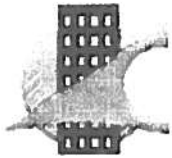
Place: Hyderabad.

Date: 12th October 2016.


M. DATTA TRI N.
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

**DESIGN REPORT FOR THE PROPOSED GROUP
HOUSING MIRYALGUDA BELONGS TO A.VASUDHA
REDDY & OTHERS**

STRUCTURAL CONSULTANTS:

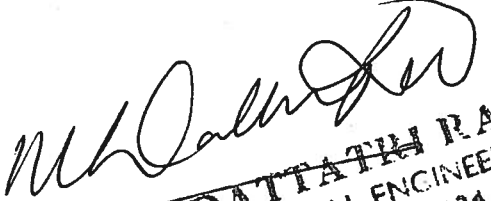


STRUCTURAL ENGINEERS, ARCHITECTS & PROJECT CONSULTANT'S
#216, KUBERA TOWER'S, NARAYAN GUDA, HYDERABAD.
CONTACT NO'S:- 04023223891, 09246343724, 09246343720.
EMAIL:- kulku kcons@yahoo.com

A handwritten signature in black ink, appearing to read 'M. Dattatri Rao'. The signature is written in a cursive, flowing style and is positioned above a horizontal line.

M. DATTATRI RAO
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

<u>S.NO</u>	<u>CONTENT</u>
1.	GENERAL
2.	SCOPE
3.	REFERENCE
4.	DESCRIPTION OF BUILDING
5.	STAAD MODELING AND DESIGN
6.	LOAD CASES
7.	LOAD COMBINATIONS
8.	STAAD INPUT
9.	STAAD OUTPUT
10.	FOUNDATION DESIGN
11.	CONCLUSION


M. DATTATH RAO
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

1.0 GENERAL:

This document covers the Load establishment, Analysis and Design of CWC Building.

2.0 SCOPE:

This document contains the Design of all RCC members including foundations.

3.0 REFERENCES:

The following codes, standards and drawings have been referred.

- a) IS: 875(1987) part 1 Dead loads
- b) IS: 875(1987) part 2 Imposed loads
- c) IS: 875(1987) part 3 Wind loads
- d) IS: 875(1987) part 5 Load combinations

4.0 DESCRIPTION OF STRUCTURE:

The structure is an RC framed structure. The structure is approximately 12.0m long x 18 m wide 17 m height. The building is covered with brick cladding on all sides.

5.0 Staad Modeling and Design:

A Three Dimensional Staad Modeling is done with most of the structural members modeled. All Members modeled is designed by In-Built facility available in Staad as per the Indian Codes. RCC members are designed as per IS 456-2000. The foundation is designed separately taking the reaction from the staad model

6.0 LOAD CASES:

Load No.	The various load cases considered are as follows:	
1.	Seismic load in X Dir (+ve) (Left to right)	SX
2.	Seismic load in X Dir (-ve) (Right to left)	-SX
3.	Seismic load in Z Dir (+ve) (Back to front)	SZ
4.	Seismic load in Z Dir (-ve) (Front to back)	-SZ
5.	Dead Load	DL
6.	Live Load	LL
7.	Wind load in X Dir (+ve) (Left to right)	WX
8.	Wind load in X Dir (-ve) (Right to left)	-WX
9.	Wind load in Z Dir (+ve) (Back to front)	WZ
10.	Wind load in Z Dir (-ve) (Front to back)	-WZ


M. DATTA RAJ
STRUCTURAL ENGINEER
GHMC. No. 184

6.1 SEISMIC LOAD

Seismic loads on the structure is considered as per the provisions of IS 1893-2002/2005.

Following cases are considered for seismic load acting along transverse frame direction

- Load case 1 seismic load acting in + X direction
- Load case 2 seismic load acting in - X direction
- Load case 3 seismic load acting in Z direction
- Load case 4 seismic load acting in -Z direction

6.5 DEAD LOAD

A. SELFWEIGHT

This Load case includes all the Dead weight of the structure, like weight of Columns, Beams, etc. Self-weight of all members modeled in STAAD is calculated by the Program.

- B. Weight of RC slab is considered as 25KN/cum
- C. Weight of brick wall is considered as 20KN/cu

6.6 LIVE LOAD

- A. On floor slab it is considered as 3KN/sqm
- B. On roof it is considered as 1.5KN/sqm

6.7 WIND LOAD

Wind loads on the structure is considered as per the provisions of IS 875-1987 (part 3).


Following cases are considered for wind load acting along transverse frame direction

- Load case 7 wind load acting in + X direction
- Load case 8 wind load acting in - X direction
- Load case 9 wind load acting in Z direction
- Load case 10 wind load acting in -Z direction

7. LOAD COMBINATIONS

FOR FOUNDATION DESIGN


1. DL + LL
2. DL + SX
3. DL - SX
4. DL + SZ
5. DL - SZ
6. DL + WX
7. DL - WX
8. DL + WZ
9. DL - WZ


M. DATTA TRIPATHI
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

10. DL + LL + SX
11. DL + LL - SX
12. DL + LL + SZ
13. DL + LL -SZ
14. DL + LL + WX
15. DL + LL -WX
16. DL + LL +WZ
17. DL + LL- WZ

The RC designs are done in staad program itself. The design is done by limit state method. Appropriate factors are multiplied for the load combination to get the desired result. The load combinations used are as follows

18. 1.5(DL + LL)
19. 1.2(DL + SX) + 0.6LL
20. 1.2(DL - SX) + 0.6LL
21. 1.2(DL + SZ) + 0.6LL
22. 1.2(DL - SZ) + 0.6LL
23. 1.5(DL + SX)
24. 1.5(DL - SX)
25. 1.5(DL + SZ)
26. 1.5(DL - SZ)
27. 0.9DL + 1.5SX
28. 0.9DL - 1.5SX
29. 0.9DL + 1.5SZ
30. 0.9DL - 1.5SZ
31. 1.2(DL + LL + WX)
32. 1.2(DL + LL - WX)
33. 1.2(DL + LL + WZ)
34. 1.2(DL + LL - WZ)
35. 1.5(DL + WX)
36. 1.5(DL - WX)
37. 1.5(DL + WZ)
38. 1.5(DL - WZ)
39. 0.9DL + 1.5WX
40. 0.9DL - 1.5WX
41. 0.9DL + 1.5WZ
42. 0.9DL - 1.5WZ


M. DATTATRAYA
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

Design Details

Project:	Amenities Block in the proposed GATED COMMUNITY LAY-OUT CUM GROUP HOUSING IN SY. 786 (P) SITUATED AT MIRYALGUDA TOWN AND MANDAL BELONGS TO SMT. A. VASUDHA REDDY & OTHERS		
Present Scope:	STILT + FOUR UPPER FLOORS		
Future Expansion:			
Total floors designed	STILT + FOUR UPPER FLOORS		

Ref. to Arch Drawings:

1	Floor Plan	Asper plans submitted to Miryalaguda Municipality
2	Elevations	Asper plans submitted to Miryalaguda Municipality
3	Sections	Asper plans submitted to Miryalaguda Municipality

Soil Particulars:

Reference to the Soil Report	As recommended by M/s. Geo Technologies		
Recommended SBC	250 kN/m ²		
N Value and Soil Type	Considered as Medium Soil		
%age of Permissible Increase in Allowable Bearing Pressure or Resistance of Soils	Piles not resting on Hard soil		25
	Raft Foundations		50
	Combined, Isolated Footings		25

Seismic Data:

Zone	II	As per Annex E IS 1893-2002 Pg 35
Zone Factor (Z):	0.1	As per Table 2 IS 1893-2002 Pg 16
Imp Factor (I)	1	As per Table 6 IS 1893-2002 Pg 18
Response Reduction Factor	3	As per Table 7 IS 1893-2002 Pg 23
Px = 0.09h/Sqrt(L)	#REF!	As per Cl 7.6.2 IS 1893-2002 Pg 24
Pz = 0.09h/Sqrt(W)	#REF!	As per Cl 7.6.2 IS 1893-2002 Pg 24
Load Considered for Seismic Weights	50	As per Table 8 IS 1893-2002 Pg 24
Structure Type	RC Frame with infills (ST = 3 in STAAD INPUT)	

(Handwritten Signature)


Lateral Wind Data:

Basic Wind Speed:		50 m/sec		Design Wind Speed $V_z = V_b \cdot K_1 \cdot K_2 \cdot K_3$	
k1 probability factor		1.0		Design Wind Pressure = $0.6 V_z^2$	
k2 Terrain (Category 3), height and structure size (Class B) factor		10m	0.88	$0.6(50 \times 1.0 \times 1.03 \times 1.0)^2 =$	1.162
		15m	0.94	$0.6(50 \times 1.0 \times 1.07 \times 1.0)^2 =$	1.325
		20m	0.98	$0.6(50 \times 1.0 \times 1.10 \times 1.0)^2 =$	1.441
k3 factor		1.0			
Ratio h/w	#REF!	Cpe	0.7	Tab 4 Cl 6.2.2.1 IS 875-Part-III Pg 14	
Ratio l/w	#REF!	Cpi	0.5	Cl 6.2.3.2 IS 875-Part-III Pg 36	
Wind Load Considered in STAAD					
Upto 10 m height		$(0.7+0.5) \times 1.591$	=	1.394	kN/m^2
From 10m to 15m height		$(0.7+0.5) \times 1.717$	=	1.590	kN/m^2
From 15m to 20m height		$(0.7+0.5) \times 1.815$	=	1.729	kN/m^2

Loading Particulars:**Dead Load**

DL on Floor Slabs	$0.15 \times 25 + 1.50(\text{FF}) = 5.625 \text{ kN/m}^2$
DL on Terrace Slab	$0.15 \times 25 + 0.15 \times 20 = 6.75 \text{ kN/m}^2$
230 Br. Wall Load	4.60 kN/m per metre Height of wall
115 Br. Wall Load	2.30 kN/m per metre Height of wall
Railing Load	1.875 kN/m per metre Height of Railing

Live Load: (As per IS 875 (Part 2) -1987)**For RESIDENTIAL Buildings**

Considered uniformly 2.0 kN/m^2
 FOR CELLAR SLABS 4 kN/m^2

Basic Load Cases:

- | | |
|---------------------------|-----|
| 1 Seismic in X-Direction | SX |
| 2 Seismic in -X-Direction | -Sx |
| 3 Seismic in Z-Direction | SZ |
| 4 Seismic in -Z-Direction | -Sz |
| 5 Dead Load | DL |
| 6 Live Load on Floors | LLF |
| 7 Wind in X-Direction | WX |
| 8 Wind in -X-Direction | -Wx |
| 9 Wind in Z-Direction | WZ |
| 10 Wind in -Z-Direction | -Wz |

M. Dattatraya Rao
M. DATTATRAYA RAO
 STRUCTURAL ENGINEER
 GHMC. Ls. No.: 134

Load Combinations Considered in the Analysis:


(Limit State of Collapse) as per IS 456-2000 Pg 68

- 11 $1.5(DL + LL)$
- 12 $1.2(DL + SX) + 0.6LL$
- 13 $1.2(DL - SX) + 0.6LL$
- 14 $1.2(DL + SZ) + 0.6LL$
- 15 $1.2(DL - SZ) + 0.6LL$
- 16 $1.5(DL + SX)$
- 17 $1.5(DL - SX)$
- 18 $1.5(DL + SZ)$
- 19 $1.5(DL - SZ)$
- 20 $0.9DL + 1.5SX$
- 21 $0.9DL - 1.5SX$
- 22 $0.9DL + 1.5SZ$
- 23 $0.9DL - 1.5SZ$
- 24 $1.2(DL + LL + WX)$
- 25 $1.2(DL + LL - WX)$
- 26 $1.2(DL + LL + WZ)$
- 27 $1.2(DL + LL - WZ)$
- 28 $1.5(DL + WX)$
- 29 $1.5(DL - WX)$
- 30 $1.5(DL + WZ)$
- 31 $1.5(DL - WZ)$
- 32 $0.9DL + 1.5WX$
- 33 $0.9DL - 1.5WX$
- 34 $0.9DL + 1.5WZ$
- 35 $0.9DL - 1.5WZ$


M. DATTATRAYA RAO
STRUCTURAL ENGINEER
SHMC. Is. No.: 154

(Limit State of Serviceability) as per IS 456-200 Pg 68

- 41 $1.0DL + 1.0LL$
- 42 $1.0 DL + 1.0SX$
- 43 $1.0 DL - 1.0SX$
- 44 $1.0 DL + 1.0Sz$
- 45 $1.0 DL - 1.0Sz$
- 46 $1.0 DL + 1.0WX$
- 47 $1.0 DL - 1.0WX$
- 48 $1.0 DL + 1.0Wz$
- 49 $1.0 DL - 1.0Wz$
- 50 $1.0 DL + 0.5 LL + 1.0SX$
- 51 $1.0 DL + 0.5 LL - 1.0SX$
- 52 $1.0 DL + 0.5 LL + 1.0Sz$
- 53 $1.0 DL + 0.5 LL - 1.0Sz$
- 54 $1.0 DL + 1.0 LL + 1.0Wx$
- 55 $1.0 DL + 1.0 LL - 1.0Wx$
- 56 $1.0 DL + 1.0 LL + 1.0Wz$
- 57 $1.0 DL + 1.0 LL - 1.0Wz$


M. D. SRINIVAS RAO
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

STAAD INPUT

STAAD SPACE

START JOB INFORMATION

ENGINEER DATE 09-Nov-16

END JOB INFORMATION

INPUT WIDTH 79

UNIT METER KN

JOINT COORDINATES

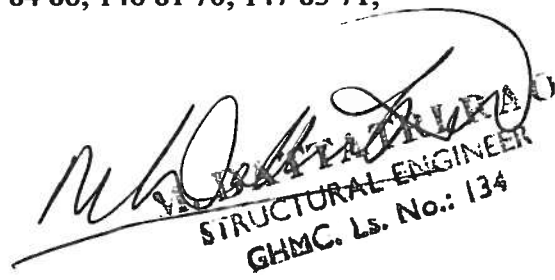
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M. H. QADRI RAO
STRUCTURAL ENGINEER
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ISOTROPIC CONCRETE

E 2.17185e+007

M. DATTANATHAN
STRUCTURAL ENGINEER
GHMC, La. No. 134

POISSON 0.17

DENSITY 23.5616

ALPHA 1e-005

DAMP 0.05

TYPE CONCRETE

STRENGTH FCU 27579

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MEMBER PROPERTY AMERICAN

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MEMBER PROPERTY

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CONSTANTS

BETA 90 MEMB 1 4 6 7 9 TO 15 17 43 46 48 49 51 TO 57 59 101 104 106 107 109 -

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MATERIAL CONCRETE ALL

SUPPORTS

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UNIT MMS NEWTON

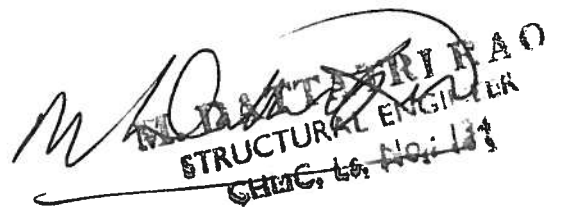
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M. A. T. P. R. I. E. A. O.
STRUCTURAL ENGINEER
SEMIC. LG. No: 111

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0.000885097 0.000895153 0.000904701 0.000913798 0.000922493 0.000930826 -

0.000938831 0.000946537 0.00095397 HEIG 0 4572 5158.15 5744.31 6330.46 -

6916.62 7502.77 8088.92 8675.08 9261.23 9847.39 10433.5 11019.7 -

11605.9 12192

EXP 0.8 JOINT 1 TO 169

DEFINE 1893 LOAD

ZONE 0.1 RF 3 I 1 SS 2 ST 1

SELFWEIGHT 1

MEMBER WEIGHT

60 TO 62 64 66 TO 71 73 TO 75 77 TO 82 84 85 87 89 90 92 94 TO 96 98 TO 100 -

118 TO 121 125 TO 129 133 TO 138 141 144 146 149 151 155 175 TO 178 -

182 TO 186 190 TO 195 198 201 203 206 208 212 232 TO 235 239 TO 243 -

247 TO 252 255 258 260 263 265 269 UNI 8

122 124 130 TO 132 139 142 147 152 TO 154 156 157 179 181 187 TO 189 196 199 -

204 213 214 236 238 244 TO 246 253 256 261 270 271 UNI 6

289 TO 291 296 TO 300 305 TO 309 312 315 317 320 322 326 UNI 2.5

FLOOR WEIGHT

YRANGE 5000 17000 FLOAD 0.004625

UNIT METER KN

LOAD 1 LOADTYPE Seismic TITLE EQ+X

1893 LOAD X 1

LOAD 2 LOADTYPE Seismic TITLE EQ-X

1893 LOAD X -1

LOAD 3 LOADTYPE Seismic TITLE EQ+Z

1893 LOAD Z 1

LOAD 4 LOADTYPE Seismic TITLE EQ-Z

1893 LOAD Z -1

LOAD 5 LOADTYPE Dead TITLE DL

SELFWEIGHT Y -1


M. H. J. K.
REGISTERED PROFESSIONAL ENGINEER

FLOOR LOAD

YRANGE 5 17 FLOAD -4.625 GY

LOAD 6 LOADTYPE Live TITLE LL

FLOOR LOAD

YRANGE 5 17 FLOAD -3 GY

LOAD 7 LOADTYPE Dead TITLE WL

MEMBER LOAD

18 TO 21 25 TO 29 34 TO 38 41 60 TO 63 67 TO 71 76 TO 81 84 87 89 92 94 98 -

118 TO 121 125 TO 129 133 TO 138 141 144 146 149 151 155 175 TO 178 -

182 TO 186 190 TO 195 198 201 203 206 208 212 232 TO 235 239 TO 243 -

247 TO 252 255 258 260 263 265 269 291 292 304 305 UNI GY -12

64 73 TO 75 85 90 99 100 122 124 130 TO 132 139 142 147 152 TO 154 156 157 -

179 181 187 TO 189 196 199 204 209 TO 211 213 214 236 238 244 TO 246 253 -

256 261 266 TO 268 270 271 UNI GY -6

289 290 296 TO 300 306 TO 309 312 315 317 320 322 325 326 UNI GY -3

LOAD 8 LOADTYPE Wind TITLE W+X

WIND LOAD X 1 TYPE 1

LOAD 9 LOADTYPE Wind TITLE W-X

WIND LOAD -X -1 TYPE 1

LOAD 10 LOADTYPE Wind TITLE W+Z

WIND LOAD Z 1 TYPE 1

LOAD 11 LOADTYPE Wind TITLE W-Z

WIND LOAD -Z -1 TYPE 1

LOAD COMB 12 GENERATED INDIAN CODE GENRAL_STRUCTURES 1

5 1.5 7 1.5 6 1.5

LOAD COMB 13 GENERATED INDIAN CODE GENRAL_STRUCTURES 2

5 1.2 7 1.2 6 1.2 8 1.2

LOAD COMB 14 GENERATED INDIAN CODE GENRAL_STRUCTURES 3

5 1.2 7 1.2 6 1.2 9 1.2

LOAD COMB 15 GENERATED INDIAN CODE GENRAL_STRUCTURES 4

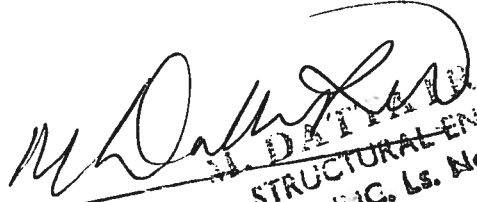
5 1.2 7 1.2 6 1.2 10 1.2

LOAD COMB 16 GENERATED INDIAN CODE GENRAL_STRUCTURES 5

5 1.2 7 1.2 6 1.2 11 1.2


M. DATTA TRI RAO
STRUCTURAL ENGINEER
GHMC. Ls. No.: 134

LOAD COMB 17 GENERATED INDIAN CODE GENRAL_STRUCTURES 6
5 1.2 7 1.2 6 1.2 8 -1.2
LOAD COMB 18 GENERATED INDIAN CODE GENRAL_STRUCTURES 7
5 1.2 7 1.2 6 1.2 9 -1.2
LOAD COMB 19 GENERATED INDIAN CODE GENRAL_STRUCTURES 8
5 1.2 7 1.2 6 1.2 10 -1.2
LOAD COMB 20 GENERATED INDIAN CODE GENRAL_STRUCTURES 9
5 1.2 7 1.2 6 1.2 11 -1.2
LOAD COMB 21 GENERATED INDIAN CODE GENRAL_STRUCTURES 10
5 1.2 7 1.2 6 1.2 1 1.2
LOAD COMB 22 GENERATED INDIAN CODE GENRAL_STRUCTURES 11
5 1.2 7 1.2 6 1.2 2 1.2
LOAD COMB 23 GENERATED INDIAN CODE GENRAL_STRUCTURES 12
5 1.2 7 1.2 6 1.2 3 1.2
LOAD COMB 24 GENERATED INDIAN CODE GENRAL_STRUCTURES 13
5 1.2 7 1.2 6 1.2 4 1.2
LOAD COMB 25 GENERATED INDIAN CODE GENRAL_STRUCTURES 14
5 1.2 7 1.2 6 1.2 1 -1.2
LOAD COMB 26 GENERATED INDIAN CODE GENRAL_STRUCTURES 15
5 1.2 7 1.2 6 1.2 2 -1.2
LOAD COMB 27 GENERATED INDIAN CODE GENRAL_STRUCTURES 16
5 1.2 7 1.2 6 1.2 3 -1.2
LOAD COMB 28 GENERATED INDIAN CODE GENRAL_STRUCTURES 17
5 1.2 7 1.2 6 1.2 4 -1.2
LOAD COMB 29 GENERATED INDIAN CODE GENRAL_STRUCTURES 18
5 1.5 7 1.5 8 1.5
LOAD COMB 30 GENERATED INDIAN CODE GENRAL_STRUCTURES 19
5 1.5 7 1.5 9 1.5
LOAD COMB 31 GENERATED INDIAN CODE GENRAL_STRUCTURES 20
5 1.5 7 1.5 10 1.5
LOAD COMB 32 GENERATED INDIAN CODE GENRAL_STRUCTURES 21
5 1.5 7 1.5 11 1.5
LOAD COMB 33 GENERATED INDIAN CODE GENRAL_STRUCTURES 22


N. DATTANATHAN
STRUCTURAL ENGINEER
CHIC. Ls. No.: 134

5 1.5 7 1.5 8 -1.5
LOAD COMB 34 GENERATED INDIAN CODE GENRAL_STRUCTURES 23
5 1.5 7 1.5 9 -1.5
LOAD COMB 35 GENERATED INDIAN CODE GENRAL_STRUCTURES 24
5 1.5 7 1.5 10 -1.5
LOAD COMB 36 GENERATED INDIAN CODE GENRAL_STRUCTURES 25
5 1.5 7 1.5 11 -1.5
LOAD COMB 37 GENERATED INDIAN CODE GENRAL_STRUCTURES 26
5 1.5 7 1.5 1 1.5
LOAD COMB 38 GENERATED INDIAN CODE GENRAL_STRUCTURES 27
5 1.5 7 1.5 2 1.5
LOAD COMB 39 GENERATED INDIAN CODE GENRAL_STRUCTURES 28
5 1.5 7 1.5 3 1.5
LOAD COMB 40 GENERATED INDIAN CODE GENRAL_STRUCTURES 29
5 1.5 7 1.5 4 1.5
LOAD COMB 41 GENERATED INDIAN CODE GENRAL_STRUCTURES 30
5 1.5 7 1.5 1 -1.5
LOAD COMB 42 GENERATED INDIAN CODE GENRAL_STRUCTURES 31
5 1.5 7 1.5 2 -1.5
LOAD COMB 43 GENERATED INDIAN CODE GENRAL_STRUCTURES 32
5 1.5 7 1.5 3 -1.5
LOAD COMB 44 GENERATED INDIAN CODE GENRAL_STRUCTURES 33
5 1.5 7 1.5 4 -1.5
LOAD COMB 45 GENERATED INDIAN CODE GENRAL_STRUCTURES 34
5 0.9 7 0.9 1 1.5
LOAD COMB 46 GENERATED INDIAN CODE GENRAL_STRUCTURES 35
5 0.9 7 0.9 2 1.5
LOAD COMB 47 GENERATED INDIAN CODE GENRAL_STRUCTURES 36
5 0.9 7 0.9 3 1.5
LOAD COMB 48 GENERATED INDIAN CODE GENRAL_STRUCTURES 37
5 0.9 7 0.9 4 1.5
LOAD COMB 49 GENERATED INDIAN CODE GENRAL_STRUCTURES 38
5 0.9 7 0.9 1 -1.5



LOAD COMB 50 GENERATED INDIAN CODE GENRAL_STRUCTURES 39

5 0.9 7 0.9 2 -1.5

LOAD COMB 51 GENERATED INDIAN CODE GENRAL_STRUCTURES 40

5 0.9 7 0.9 3 -1.5

LOAD COMB 52 GENERATED INDIAN CODE GENRAL_STRUCTURES 41

5 0.9 7 0.9 4 -1.5

PERFORM ANALYSIS

PRINT ANALYSIS RESULTS

START CONCRETE DESIGN

CODE INDIAN

CLEAR 0.025 ALL

FC 20000 MEMB 18 TO 42 60 TO 71 73 TO 100 118 TO 157 175 TO 214 232 TO 271 -
289 TO 328

FC 25000 MEMB 1 TO 17 43 TO 59 101 TO 117 158 TO 174 215 TO 231 272 TO 288

FYMAIN 500000 ALL

FYSEC 415000 ALL

MAXMAIN 20 ALL

MAXSEC 12 ALL

MINMAIN 10 ALL

MINSEC 8 ALL

DESIGN BEAM 18 TO 42 60 TO 71 73 TO 100 118 TO 157 175 TO 214 232 TO 271
289 -

290 TO 328

DESIGN COLUMN 1 TO 17 43 TO 59 101 TO 117 158 TO 174 215 TO 231 272 TO
288

END CONCRETE DESIGN

PRINT JOINT COORDINATES

PRINT MEMBER INFORMATION

PRINT SUPPORT REACTION

FINISH

M. DATTATRI PAO
STRUCTURAL ENGINEER
GHMC. Ls. No.: 137

DESIGN OF FLAT FOOTING

LOAD DATA

Unfactored Load P = 2800 KN
 Unfactored MOM-Mx = 1.94 KN-m
 Unfactored MOM-My = 0.084 KN-m
 SBC = 250

Dimensions of

Cx = 0.23
 Cy = 0.6

Fck = 20 N/Sqmm
 Fy = 115 N/Sqmm

STABILITY CHECK - Check for Stresses

Area of the Footing Required = 4.54 Sqm.
 Footing Size Required = 2.35 each side
 However Provide
 Fx = 2.4 m
 Fy = 2.4 m
 Area Provided = 5.76 Sqm.
OK

RESPECT PADO

Zx = 2.30 Cum
 Zy = 2.30 Cum

$$f = P/A + Mx/Zx + My/Zy$$

Fmax = 382.82 KN/m²
 < 400 KN/m²

Fmin = 361.07 KN/m²

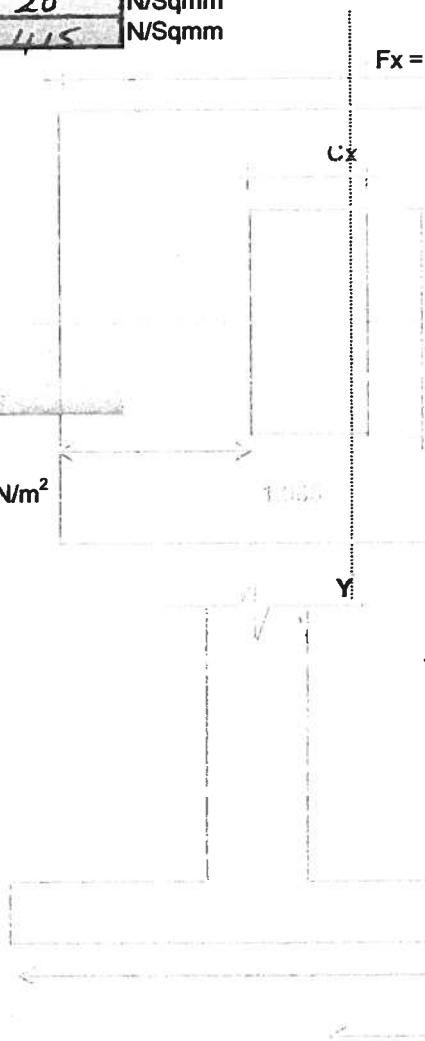
Net Upward Pressure = 348.10 KN/Sqm

D = 0.75 m
 d = 0.7 m

S F in X dir @ d = 18.1151 KN
 S F in Y dir @ d = 18.2051 KN

Shear Stress (Tvx) in X = 0.78 N/Sqmm

Shear Stress (Tvy) in Y = 0.78 N/Sqmm



DEPTH OF FOOTING REQUIRED AS PER MOMENT

For 1.94 Cantilever

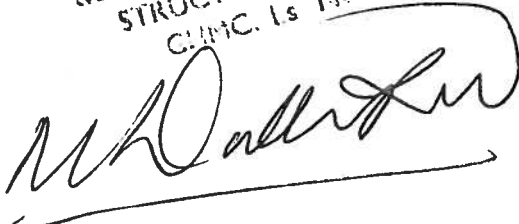
Moment = 204.90 KN-m
 Mu = 245.88

$$d = (\text{SQRT}(\text{Mu}/0.138f_{ct}b))$$

d = 0.30

CHECK FOR SHEAR STRESSES

M. DATTA TRIPATHI
 STRUCTURAL ENGINEER
 C/M.C. Is No: 134



The critical section for one way shear is taken at a distance equal to the effective depth from the column

Shear Force at critical section along X direction

SFu X = kN

Shear Force at critical section along Z direction

SFu Z = kN

$q_{vx} = \frac{385.98}{4460} = 0.23 \text{ N/sqmm}$
 $q_{vz} = \frac{200.51}{4460} = 0.12 \text{ N/sqmm}$

$< q_c$
 FROM SP 16

The critical section for two way shear is taken at a distance equal to half the effective depth from the col

$d/2 = \frac{4460}{2} = 2230 \text{ mm} = 2.23 \text{ m}$
 $(b+a) = 0.93 \text{ m}$
 $(d+a) = 1.30 \text{ m}$
 $b_0 = 4460.00 \text{ mm}$

$a = 0.7 \text{ m}$

Shear Force at this critical section = $S_u = 1584210.21 \text{ N}$

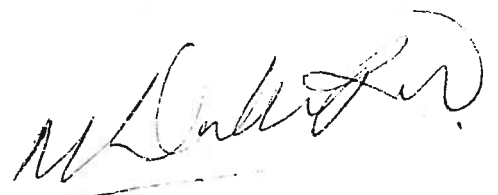
$q_v = 0.76 \text{ N/sqmm}$

$\beta_c = \frac{\text{short side of the column}}{\text{long side of the column}} = 0.38$

$K_s = 0.5 + \beta_c = 0.88$
 But K_s is limited to 1.00 0.88333333

$q_c = K_s \times 0.25 \times \sqrt{f_{ck}} = 0.9876 \text{ N/sqmm}$

For	Cantilever	WIDTH
Moment =	<input type="text"/>	KN-m
$M_u/bD^2 =$	<input type="text"/>	
Pt =	<input type="text"/>	
$A_{st_reqd.} =$	<input type="text"/>	Sqmm
Provided	<input type="text"/>	@ <input type="text"/> mm c/c
NO OF BARS	<input type="text"/>	
$A_{st_provd.} =$	<input type="text"/>	Sqmm

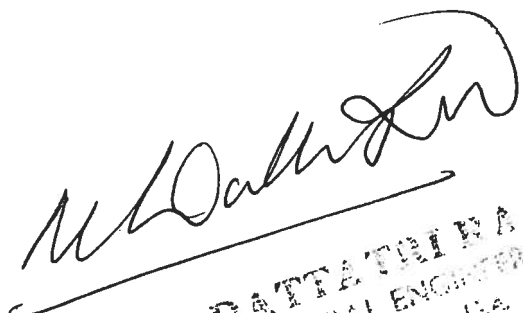


CONCLUSION

The proposed group housing Miryalguda building was analyzed by using STAAD pro software. The design of all the super structure members was done using STAAD pro software only.

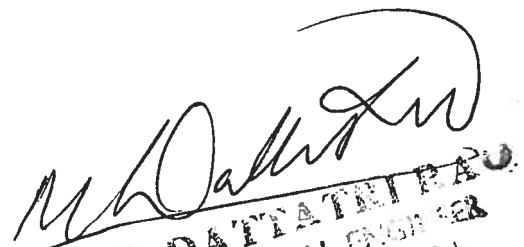
- Columns and beams are designed as per STAAD.
- Foundations are designed using spread sheet.
- Slabs are designed using spread sheet.

Hence it can be concluded that the group housing Miryalguda building structure is safe and stable for the purpose for which it is intended. It is recommended that no additional loads shall be applied on the structure.


M. DATTA TRIPATHY
STRUCTURAL ENGINEER
CHNC. Ls. No.: 134

SUPPORT REACTIONS DETAILS

Node No	Load Case	Fx	Fy	Fz	Mx	My	Mz
1							
	12	14.67	871.85	8.12	7.76	0.53	9.11
	13	6.19	672.56	5.01	2.15	0.09	0.72
	14	17.28	722.4	7.98	10.27	0.76	15.29
	15	12.02	663.71	5.67	18.66	0.31	7.71
	16	11.45	731.24	18.66	31.08	0.54	6.86
	17	17.28	722.4	7.98	10.27	0.76	15.29
	18	6.19	672.56	5.01	2.15	0.09	0.72
	32	15.38	802.88	22.24	36.76	0.53	9.35
	33	22.67	791.82	8.89	10.75	0.81	19.89
	34	8.81	729.53	5.18	0.59	0.03	0.13
	35	15.38	802.88	22.24	36.76	0.53	9.35
	36	16.09	718.46	8.17	25.42	0.24	10.41
	37	3.73	668.69	2.52	6.7	0.12	13.61
	38	27.74	852.65	11.55	18.04	0.9	33.37
	42	3.73	668.69	2.52	6.7	0.12	13.61
	43	15.57	958.35	43.71	108.86	0.18	9.76
	44	15.91	562.99	29.64	97.52	0.59	10
	45	2.56	364.42	0.29	8.97	0.28	17.57
3							
	12	11.02	1215.93	3.08	2.83	0.24	11.07
	13	28.17	954.47	2.45	2.2	0.25	55.08
	14	10.54	991.01	2.47	2.33	0.14	37.38
	15	7.86	963.06	3.95	2.93	0.27	6.63
	16	9.77	982.42	8.88	7.45	0.66	11.08
	17	10.54	991.01	2.47	2.33	0.14	37.38
	18	28.17	954.47	2.45	2.2	0.25	55.08
	19	9.77	982.42	8.88	7.45	0.66	11.08
	20	7.86	963.06	3.95	2.93	0.27	6.63
	21	52.76	916.53	2.51	2.22	0.34	119.41
	22	35.13	1028.95	2.42	2.3	0.05	101.7
	23	9.06	933.51	9.94	15.94	0.33	8.91
	24	8.57	1011.97	14.87	20.46	0.05	8.8
	25	35.13	1028.95	2.42	2.3	0.05	101.7
	26	52.76	916.53	2.51	2.22	0.34	119.41
	27	8.57	1011.97	14.87	20.46	0.05	8.8
	28	9.06	933.51	9.94	15.94	0.33	8.91
	29	35.25	1006.85	2.23	1.95	0.25	67.78
	30	13.14	1052.53	2.26	2.11	0.1	47.78


M. DATTA TRIPATHI
 CIVIL ENGINEER
 No. 154

31	9.86	1017.59	5.77	4.46	0.41	7.22
32	12.25	1041.79	10.26	8.52	0.76	12.78
33	13.14	1052.53	2.26	2.11	0.1	47.78
34	35.25	1006.85	2.23	1.95	0.25	67.78
35	12.25	1041.79	10.26	8.52	0.76	12.78
36	9.86	1017.59	5.77	4.46	0.41	7.22
37	65.99	959.43	2.3	1.98	0.36	148.19
38	43.88	1099.95	2.19	2.08	0.01	128.2
39	11.36	980.65	13.26	20.72	0.35	10.07
40	10.75	1078.73	17.75	24.78	0	9.93
41	43.88	1099.95	2.19	2.08	0.01	128.2
42	65.99	959.43	2.3	1.98	0.36	148.19
43	10.75	1078.73	17.75	24.78	0	9.93

5

12	9.61	672.47	6.74	6.08	0.44	7.93
13	21.08	504.91	5.45	4.96	0.11	29.39
14	5.71	571.04	5.33	4.76	0.6	16.7
15	6.96	506.82	1.85	1.48	0.03	5.17
16	8.41	569.13	12.63	11.21	0.74	7.52
17	5.71	571.04	5.33	4.76	0.6	16.7
18	21.08	504.91	5.45	4.96	0.11	29.39
19	8.41	569.13	12.63	11.21	0.74	7.52
20	6.96	506.82	1.85	1.48	0.03	5.17
21	38.93	442.25	5.65	5.36	0.01	61.67
22	23.56	633.7	5.13	4.36	0.7	48.99
23	7.81	404.53	4.6	9.29	0.28	6.41
24	7.56	671.42	15.38	19.02	0.43	6.28
25	23.56	633.7	5.13	4.36	0.7	48.99
26	38.93	442.25	5.65	5.36	0.01	61.67
27	7.56	671.42	15.38	19.02	0.43	6.28
28	7.81	404.53	4.6	9.29	0.28	6.41
29	25.86	561.7	5.51	4.87	0.02	35.92
30	7.64	644.36	5.37	4.63	0.64	21.7
31	8.2	564.09	3.61	3.18	0.15	5.64
32	10.02	641.98	14.48	12.68	0.8	8.58
33	7.64	644.36	5.37	4.63	0.64	21.7
34	25.86	561.7	5.51	4.87	0.02	35.92
35	10.02	641.98	14.48	12.68	0.8	8.58
36	8.2	564.09	3.61	3.18	0.15	5.64
37	48.17	483.37	5.76	5.37	0.11	76.28
38	29.95	722.69	5.12	4.12	0.76	62.05

7

12	2.79	441.51	5.76	5.69	0.67	2.34
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A handwritten signature in black ink, appearing to read 'M. W. ...', is located in the bottom right corner of the page. The signature is written in a cursive style and is positioned over a faint, illegible stamp or background text.

13	8.13	424.81	5.73	6.75	0.22	9.58
14	3.66	281.6	3.49	2.35	0.85	5.83
15	1.93	307.08	2.34	7.83	0.14	1.48
16	2.53	399.34	11.55	16.92	0.94	2.26
17	3.66	281.6	3.49	2.35	0.85	5.83
18	8.13	424.81	5.73	6.75	0.22	9.58
19	2.53	399.34	11.55	16.92	0.94	2.26
20	1.93	307.08	2.34	7.83	0.14	1.48
21	16.21	562.56	7.01	9.5	0.11	20.41
22	11.74	143.85	2.2	0.4	0.96	16.67
23	2.39	160.68	14.45	35.36	0.43	1.97
24	2.08	545.73	23.66	44.46	0.65	1.77
25	11.74	143.85	2.2	0.4	0.96	16.67
26	16.21	562.56	7.01	9.5	0.11	20.41
42	19.91	664.61	7.59	10.42	0.03	25.15
43	2.25	643.58	28.4	54.11	0.64	1.85

9

12	3.83	1049.77	0.08	1.75	0.53	4.82
13	13.97	791.26	0.65	1.85	0.16	24.01
14	20.1	888.37	0.52	0.95	0.69	31.73
15	1.89	866.3	4.79	4.92	0.14	2.38
16	4.23	813.33	4.92	7.72	0.7	5.34
17	20.1	888.37	0.52	0.95	0.69	31.73
18	13.97	791.26	0.65	1.85	0.16	24.01
19	4.23	813.33	4.92	7.72	0.7	5.34
20	1.89	866.3	4.79	4.92	0.14	2.38
21	31.59	702.28	1.46	2.65	0.08	55.98
22	37.72	977.36	1.33	0.15	0.77	63.7
23	3.81	946.74	9.91	12.74	0.33	4.11
24	2.32	732.9	10.04	15.54	0.52	3.61
25	37.72	977.36	1.33	0.15	0.77	63.7
26	31.59	702.28	1.46	2.65	0.08	55.98
27	2.32	732.9	10.04	15.54	0.52	3.61
28	3.81	946.74	9.91	12.74	0.33	4.11
29	18.36	792.85	0.23	1.44	0.06	31.22
30	24.23	914.23	1.24	0.32	0.72	38.45
31	1.47	886.65	6.57	7.02	0.04	1.77
32	4.39	820.44	5.56	8.78	0.74	5.46
41	46.25	1025.47	2.26	0.68	0.82	78.42
42	40.38	681.62	1.24	2.44	0.04	71.19
43	2	719.89	11.96	18.56	0.51	3.31
44	3.87	987.19	12.98	16.8	0.27	3.92

11

M. S. S. S. S. S.
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12	0.01	1183.8	25.95	20.13	0.82	0.82
13	8.07	1022.47	22.75	20.82	0.12	10.64
14	8.06	871.61	18.76	11.39	1.19	11.96
15	0.65	986.07	9.18	10.68	0.13	0.02
16	0.64	908.01	32.34	42.89	1.18	1.34
17	8.06	871.61	18.76	11.39	1.19	11.96
18	8.07	1022.47	22.75	20.82	0.12	10.64
19	0.64	908.01	32.34	42.89	1.18	1.34
20	0.65	986.07	9.18	10.68	0.13	0.02
21	16.73	1170.88	25.09	26.82	0.05	23.67
22	16.72	723.2	16.42	5.39	1.37	24.98
23	0.22	1115.76	14.85	71.12	0.51	0.44
24	0.21	778.32	56.36	103.33	0.81	0.87
25	16.72	723.2	16.42	5.39	1.37	24.98
26	16.73	1170.88	25.09	26.82	0.05	23.67
27	0.21	778.32	56.36	103.33	0.81	0.87
28	0.22	1115.76	14.85	71.12	0.51	0.44
29	10.51	1113.41	28.93	24.56	0.06	13.8
30	9.66	924.83	23.94	12.78	1.28	14.46
31	1.23	1067.91	11.96	14.81	0.04	0.52
32	0.38	970.33	40.91	52.15	1.27	1.18
41	20.48	739.32	21.01	5.28	1.5	30.74
42	21.33	1298.92	31.85	32.06	0.28	30.07
43	0.16	808.22	70.94	127.7	0.8	0.6
44	0.7	1230.01	18.07	90.37	0.42	0.06

13

12	3.44	1558.75	14.2	12.2	0.52	0.79
13	15.14	1225.39	9.43	4.45	0.98	19.1
14	9.64	1268.61	13.3	15.06	1.81	20.37
15	2.78	1269.47	1.27	22.12	0.66	0.36
16	2.73	1224.53	24	41.63	0.17	0.9
17	9.64	1268.61	13.3	15.06	1.81	20.37
18	15.14	1225.39	9.43	4.45	0.98	19.1
19	2.73	1224.53	24	41.63	0.17	0.9
20	2.78	1269.47	1.27	22.12	0.66	0.36
21	18.54	1177.91	6.65	3.18	1.69	39.65
22	13.03	1316.09	16.08	22.7	2.53	40.92
23	3.02	1351.1	28.12	98.83	0.51	0.29
24	2.48	1142.9	50.85	118.35	0.32	0.98
25	13.03	1316.09	16.08	22.7	2.53	40.92
26	18.54	1177.91	6.65	3.18	1.69	39.65
27	2.48	1142.9	50.85	118.35	0.32	0.98
28	3.02	1351.1	28.12	98.83	0.51	0.29
29	17.24	1249.36	11.86	3.72	1.36	23.67

M. L. Carter

30	13.73	1303.39	16.7	16.99	2.13	25.66
31	1.79	1304.46	1.51	29.48	0.69	0.66
32	1.73	1248.28	30.07	50.2	0.08	1.33
41	17.98	1362.74	20.17	26.53	3.02	51.35
42	21.49	1190	8.39	5.82	2.25	49.36
43	1.42	1146.24	63.63	146.1	0.27	1.43
44	2.09	1406.5	35.07	125.38	0.5	0.56
45	20.79	679.45	2.67	9.96	2.4	49.76
46	18.68	852.19	14.46	22.39	2.86	50.95

15

12	7.32	2219.97	8.67	3.77	0.17	10.21
13	21.33	1774.25	6.36	2.78	0.98	62.19
14	33.04	1777.7	7.5	3.26	0.71	78.53
15	6.63	1776.8	15.38	16.03	0.68	7.65
16	5.07	1775.15	1.52	9.99	0.41	8.68
17	33.04	1777.7	7.5	3.26	0.71	78.53
18	21.33	1774.25	6.36	2.78	0.98	62.19
19	5.07	1775.15	1.52	9.99	0.41	8.68
20	6.63	1776.8	15.38	16.03	0.68	7.65
21	48.2	1771.7	5.23	2.07	1.57	142.92
22	59.9	1780.24	8.64	3.97	1.3	159.26
23	6.77	1767.31	26.04	37.94	0.19	7.92
24	4.93	1784.63	12.17	31.91	0.09	8.42
25	59.9	1780.24	8.64	3.97	1.3	159.26
26	48.2	1771.7	5.23	2.07	1.57	142.92
27	4.93	1784.63	12.17	31.91	0.09	8.42
28	6.77	1767.31	26.04	37.94	0.19	7.92
29	29.05	1621.86	4.99	2.11	1.2	80.93
30	38.91	1626.17	6.42	2.72	0.92	94.97
31	5.9	1625.04	16.26	18.68	0.83	6.38
32	3.95	1622.98	4.86	13.84	0.54	7.66
41	72.49	1629.35	7.83	3.61	1.65	195.88
42	62.63	1618.68	3.57	1.23	1.94	181.84
43	3.77	1634.84	18.18	41.24	0.08	7.33
44	6.08	1613.19	29.58	46.07	0.21	6.71
45	64.61	969.07	1.29	0.26	1.88	184.65
46	70.52	979.74	5.55	2.64	1.71	193.07

17

12	3.15	1725.95	2.39	0.85	0.06	1.28
13	17.53	1354.51	3.42	4.71	0.46	18.61
14	12.5	1407.01	0.41	3.35	0.37	16.56
15	2.69	1378.65	11.15	24.53	0.01	1.32
16	2.35	1382.87	7.32	23.17	0.11	0.73

M. Walker

17	12.5	1407.01	0.41	3.35	0.37	16.56
18	17.53	1354.51	3.42	4.71	0.46	18.61
19	2.35	1382.87	7.32	23.17	0.11	0.73
20	2.69	1378.65	11.15	24.53	0.01	1.32
21	18.93	1298.89	5.6	10.58	0.89	31.68
22	13.9	1462.63	1.77	9.22	0.79	29.63
23	2.59	1372.47	32.27	84.17	0.05	1.13
24	2.44	1389.06	28.44	82.81	0.14	0.92
25	13.9	1462.63	1.77	9.22	0.79	29.63
26	18.93	1298.89	5.6	10.58	0.89	31.68
27	2.44	1389.06	28.44	82.81	0.14	0.92
28	2.59	1372.47	32.27	84.17	0.05	1.13
29	19.84	1342.37	4.72	6.67	0.57	22.14
30	17.69	1408	0.96	3.4	0.47	21.83
31	1.28	1372.55	14.38	31.44	0.02	0.53
32	0.86	1377.82	8.71	28.18	0.13	0.22
41	19.44	1477.53	1.76	10.74	1	38.16
42	21.59	1272.84	7.44	14	1.1	38.47
43	0.98	1385.56	35.1	102.73	0.17	0.02
44	1.17	1364.81	40.78	106	0.07	0.28
45	21.16	722.77	6.31	13.35	1.08	38.41
46	19.87	927.45	2.9	11.39	1.02	38.22

19

12	0.8	2856.91	1.69	2.81	0.09	1.13
13	20.24	2286.67	0.73	2.83	0.77	36.06
14	21.53	2284.38	1.97	1.66	0.62	37.87
15	0.26	2282.16	13.93	39.27	0.01	0.23
16	1.03	2288.89	16.63	34.77	0.16	1.57
17	21.53	2284.38	1.97	1.66	0.62	37.87
18	20.24	2286.67	0.73	2.83	0.77	36.06
19	1.03	2288.89	16.63	34.77	0.16	1.57
20	0.26	2282.16	13.93	39.27	0.01	0.23
21	33.98	2290.24	0.49	3.15	1.54	65.61
22	35.26	2280.82	2.21	1.34	1.39	67.41
23	0.38	2268.64	36.33	116.19	0.04	0.61
24	0.91	2302.41	39.03	111.7	0.11	1.2
25	35.26	2280.82	2.21	1.34	1.39	67.41
26	33.98	2290.24	0.49	3.15	1.54	65.61
27	0.91	2302.41	39.03	111.7	0.11	1.2
28	0.38	2268.64	36.33	116.19	0.04	0.61
29	25.49	2010.36	0.49	2.46	0.95	45.27
30	26.72	2007.5	2.04	1	0.8	47.15
31	0.13	2004.73	17.83	48	0.03	0.1
32	1.1	2013.13	20.37	44.55	0.18	1.78

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42	0.95	2030.04	48.37	140.71	0.12	1.31
43	0.28	1987.82	45.84	144.16	0.03	0.57
44	42.91	1211.25	0.32	2.17	1.88	82.57
45	43.65	1199.47	1.84	0.1	1.79	83.7
46	0.04	1184.25	46.34	143.47	0	0.19
47	0.7	1226.47	47.86	141.4	0.09	0.94

21

12	1.82	1953.42	9.31	4.53	0.28	0.69
13	14.93	1589.75	5.59	1.87	1.01	33.28
14	17.85	1535.72	9.31	9.11	0.57	34.39
15	1.12	1558.25	19.34	35.9	0.14	0.11
16	1.8	1567.22	4.44	28.66	0.31	1.22
17	17.85	1535.72	9.31	9.11	0.57	34.39
18	14.93	1589.75	5.59	1.87	1.01	33.28
19	1.8	1567.22	4.44	28.66	0.31	1.22
20	1.12	1558.25	19.34	35.9	0.14	0.11
21	25.1	1645.74	3.16	9.29	1.88	60.79
22	28.02	1479.73	11.74	16.54	1.43	61.9
23	1.22	1541.18	44.85	111.22	0.32	0.22
24	1.7	1584.29	29.95	103.98	0.13	0.88
25	28.02	1479.73	11.74	16.54	1.43	61.9
26	25.1	1645.74	3.16	9.29	1.88	60.79
27	1.7	1584.29	29.95	103.98	0.13	0.88
28	1.22	1541.18	44.85	111.22	0.32	0.22
29	20.21	1583.84	7.98	1.56	1.19	42.25
30	20.76	1516.3	12.62	12.17	0.78	42.34
31	0.15	1544.46	25.17	45.66	0.1	0.78
32	0.7	1555.67	4.57	35.04	0.31	0.87
41	33.47	1446.31	15.66	21.45	1.87	76.72
42	32.92	1653.82	4.93	10.84	2.27	76.63
43	0.57	1577.01	36.45	129.19	0.08	0.46
44	0.02	1523.12	57.05	139.81	0.33	0.37
45	33.03	1033.8	0.82	12.96	2.19	76.65
46	33.36	826.28	11.54	19.33	1.95	76.71
47	0.13	903.09	52.93	137.68	0.25	0.38
48	0.46	956.99	40.57	131.32	0	0.44

23

12	1.02	1314.57	12.25	8.48	0.03	0.08
13	13.74	1020.29	11.46	10.85	0.56	16.66
14	12.11	1083.03	8.15	2.72	0.61	16.52
15	0.86	1025.39	19.75	30.9	0.02	0.14

M. D. Walker
 DATE: _____

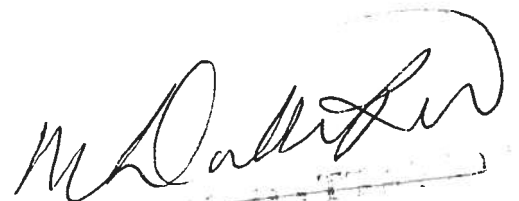
15	0.23	1043.69	20.41	32.02	0.02	0.26
16	0.06	1098.3	0.51	18.78	0.05	0.04
17	8.89	1040.75	11.59	10.89	0.6	15.89
18	9.17	1101.23	8.32	2.35	0.53	16.19
19	0.06	1098.3	0.51	18.78	0.05	0.04
20	0.23	1043.69	20.41	32.02	0.02	0.26
21	16.94	1161.07	6.1	3.55	0.48	32.11
22	16.66	980.91	13.8	16.79	0.55	31.81
23	0.26	950.28	43.62	92.14	0.06	0.21
24	0.03	1191.7	23.72	78.9	0.01	0.09
25	16.66	980.91	13.8	16.79	0.55	31.81
26	16.94	1161.07	6.1	3.55	0.48	32.11
27	0.03	1191.7	23.72	78.9	0.01	0.09
28	0.26	950.28	43.62	92.14	0.06	0.21
29	12.52	1125.47	10.55	2.56	0.68	20.86
30	10.05	1049.87	14.63	13.24	0.73	19.24
31	1.34	1053.53	25.67	39.65	0.01	0.94
32	1.13	1121.8	0.48	23.85	0.04	0.67

29

12	16.17	807.25	6.86	5.29	0	10.83
13	5.57	624.92	6.94	8.16	0.63	3.48
14	20.31	666.67	4.03	0.3	0.64	20.82
15	12.94	685.31	14.52	27.72	0.05	8.67
16	12.94	606.28	3.55	19.26	0.06	8.66
17	20.31	666.67	4.03	0.3	0.64	20.82
18	5.57	624.92	6.94	8.16	0.63	3.48
19	12.94	606.28	3.55	19.26	0.06	8.66
20	12.94	685.31	14.52	27.72	0.05	8.67
21	0.64	580.45	9.1	13.98	0.65	18.7
22	26.51	711.14	1.88	5.52	0.65	36.03
23	12.97	828.54	36.1	87.88	0.14	8.76
24	12.91	463.06	25.13	79.42	0.14	8.57
25	26.51	711.14	1.88	5.52	0.65	36.03
26	0.64	580.45	9.1	13.98	0.65	18.7
27	12.91	463.06	25.13	79.42	0.14	8.57
28	12.97	828.54	36.1	87.88	0.14	8.76
29	7.77	683.66	7.89	9.59	0.79	3.91
30	26.2	735.84	4.25	0.23	0.8	26.46
31	16.99	759.15	17.36	34.05	0.06	11.28
32	16.98	660.35	5.23	24.68	0.08	11.27

31

12	2.89	1422.08	3.74	5.17	0.01	2.91
13	32.04	1138.76	3.17	4.28	0.66	88.16



14	36.66	1136.57	2.81	3.99	0.68	92.8
15	2.28	1178.09	8.35	14.45	0.04	2.34
16	2.34	1097.23	2.38	6.18	0.06	2.31
17	36.66	1136.57	2.81	3.99	0.68	92.8
18	32.04	1138.76	3.17	4.28	0.66	88.16
19	2.34	1097.23	2.38	6.18	0.06	2.31
20	2.28	1178.09	8.35	14.45	0.04	2.34
21	71.59	1141.23	3.35	4.46	0.57	203.79
22	76.21	1134.1	2.62	3.81	0.58	208.44
23	2.35	1336.47	18.93	37.88	0.02	2.96
24	2.28	938.86	12.95	29.61	0.04	1.69
25	76.21	1134.1	2.62	3.81	0.58	208.44
26	71.59	1141.23	3.35	4.46	0.57	203.79
27	2.28	938.86	12.95	29.61	0.04	1.69
28	2.35	1336.47	18.93	37.88	0.02	2.96
29	40.32	1210.57	2.52	3.49	0.82	110.46
30	45.55	1207.83	2.07	3.13	0.85	115.74
31	2.58	1259.73	9	16.21	0.05	2.66
32	2.66	1158.66	4.41	9.58	0.08	2.62

33

12	18.29	837.73	7.11	5.16	0.04	11.92
13	20.76	688.08	4.24	0.02	0.57	21.5
14	8.51	652.29	7.14	8.28	0.64	2.42
15	14.67	712.04	15.21	28.89	0.04	9.57
16	14.6	628.32	3.83	20.63	0.03	9.51
17	8.51	652.29	7.14	8.28	0.64	2.42
18	20.76	688.08	4.24	0.02	0.57	21.5
19	14.6	628.32	3.83	20.63	0.03	9.51
20	14.67	712.04	15.21	28.89	0.04	9.57
21	27.96	726.03	2.27	5.76	0.62	36.79
22	1.3	614.34	9.1	14.02	0.69	17.71
23	14.72	855.56	36.36	87.68	0.15	9.56
24	14.55	484.8	24.99	79.42	0.08	9.52
25	1.3	614.34	9.1	14.02	0.69	17.71
26	27.96	726.03	2.27	5.76	0.62	36.79
27	14.55	484.8	24.99	79.42	0.08	9.52
28	14.72	855.56	36.36	87.68	0.15	9.56
29	26.51	757.62	4.34	1.04	0.74	27.18
30	11.19	712.89	7.97	9.33	0.78	2.72
31	18.9	787.58	18.05	35.09	0.03	12.27
32	18.8	682.93	5.75	26.81	0.01	12.19

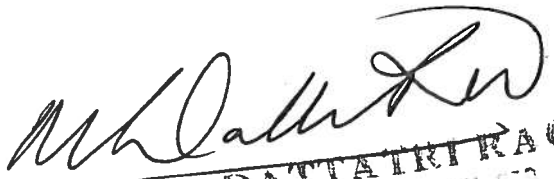

M. DATTATRI RAO
 STRUCTURAL ENGINEER
 M.C. Ls. No.: 137

COLUMN MEMBER INFORMATION

Memb No	Ast	Column Type	Reinforcement Distribution	% of Steel	Lateral Ties
1					
2	1104	TENSION COLUMN	Equal	0.98	8@190c/c
3	1104	TENSION COLUMN	Equal	0.98	8@190c/c
4	828	TENSION COLUMN	Equal	0.87	8@190c/c
5	910.8	TENSION COLUMN	Equal	1.31	8@190c/c
6	1397.95	SHORT COLUMN	Equal	1.55	8@230c/c
7	1104	TENSION COLUMN	Equal	0.98	8@190c/c
8	1440	TENSION COLUMN	Equal	0.89	8@255c/c
9	1987.37	SHORT COLUMN	Equal	1.26	8@190c/c
10	1876.8	SHORT COLUMN	Equal	1.75	8@230c/c
11	4116.66	SHORT COLUMN	Equal	2.79	8@300c/c
12	1440	TENSION COLUMN	Equal	0.89	8@255c/c
13	1104	TENSION COLUMN	Equal	0.98	8@190c/c
14	1872	SHORT COLUMN	Equal	1.26	8@190c/c
15	1104	TENSION COLUMN	Equal	0.98	8@190c/c
16	1104	TENSION COLUMN	Equal	0.98	8@190c/c
17	2247.4	SHORT COLUMN	Equal	1.26	8@190c/c
43	1104	TENSION COLUMN	Equal	0.98	8@190c/c
44	1104	TENSION COLUMN	Equal	0.98	8@190c/c
45	1104	TENSION COLUMN	Equal	0.98	8@190c/c
46	1021.2	SHORT(Z) /BRACED LONG(Y)	Equal	1.31	8@190c/c
47	828	TENSION COLUMN	Equal	0.87	8@190c/c
48	1345	SHORT(Z) /BRACED LONG(Y)	Equal	1.31	8@190c/c
49	1104	TENSION COLUMN	Equal	0.98	8@190c/c
50	1440	TENSION COLUMN	Equal	0.89	8@255c/c
51	2736	SHORT COLUMN	Equal	1.79	8@255c/c
52	2002.66	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
53	3924.39	SHORT COLUMN	Equal	2.79	8@300c/c
54	1440	TENSION COLUMN	Equal	0.89	8@255c/c
55	1385.27	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
56	1872	SHORT COLUMN	Equal	1.26	8@190c/c
57	1104	TENSION COLUMN	Equal	0.98	8@190c/c
58	1577.41	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
59	1440	TENSION COLUMN	Equal	0.89	8@255c/c
101	1505.71	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
102	1245.24	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
103	1104	TENSION COLUMN	Equal	0.98	8@190c/c
104	995.2	SHORT(Z) /BRACED LONG(Y)	Equal	1.31	8@190c/c


M. DATTATRI
 STRUCTURAL ENGINEER

105	828	TENSION COLUMN	Equal	0.87	8@190c/c
106	828	TENSION COLUMN	Equal	0.87	8@190c/c
107	1233.79	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
108	1440	TENSION COLUMN	Equal	0.89	8@255c/c
109	3393.13	SHORT COLUMN	Equal	2.09	8@300c/c
110	2197.78	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
111	2016	SHORT COLUMN	Equal	1.26	8@190c/c
112	1666.54	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
113	2067.43	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
114	1440	TENSION COLUMN	Equal	0.89	8@255c/c
115	1722.04	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
116	1886.47	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
117	1440	TENSION COLUMN	Equal	0.89	8@255c/c
158	1732.41	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
159	1389.67	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
160	1104	TENSION COLUMN	Equal	0.98	8@190c/c
161	861.9	SHORT(Z) /BRACED LONG(Y)	Equal	0.87	8@190c/c
162	828	TENSION COLUMN	Equal	0.87	8@190c/c
163	828	TENSION COLUMN	Equal	0.87	8@190c/c
164	1214.93	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
165	1440	TENSION COLUMN	Equal	0.89	8@255c/c
166	2101.25	SHORT COLUMN	Equal	1.26	8@190c/c
167	1600.67	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
168	1440	TENSION COLUMN	Equal	0.89	8@255c/c
169	1327.74	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
170	2036.1	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
171	1440	TENSION COLUMN	Equal	0.89	8@255c/c
172	1753.41	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
173	1677.04	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
174	1440	TENSION COLUMN	Equal	0.89	8@255c/c
215	1665.6	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
216	1513.61	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
217	1104	TENSION COLUMN	Equal	0.98	8@190c/c
218	828	TENSION COLUMN	Equal	0.87	8@190c/c
219	828	TENSION COLUMN	Equal	0.87	8@190c/c
220	828	TENSION COLUMN	Equal	0.87	8@190c/c
221	1195.52	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
222	1523.25	SHORT COLUMN	Equal	0.89	8@255c/c
223	1733.55	SHORT COLUMN	Equal	1.01	8@190c/c
224	1184.32	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
225	1440	TENSION COLUMN	Equal	0.89	8@255c/c
226	1104	TENSION COLUMN	Equal	0.98	8@190c/c
227	1974.45	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
228	1440	TENSION COLUMN	Equal	0.89	8@255c/c
229	1841.58	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c


M. DATTATRAYA RAO
 STRUCTURAL ENGINEER
 124


230	1554.75	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
231	1440	TENSION COLUMN	Equal	0.89	8@255c/c
272	1593.7	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
273	1464.11	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
274	1104	TENSION COLUMN	Equal	0.98	8@190c/c
275	828	TENSION COLUMN	Equal	0.87	8@190c/c
276	828	TENSION COLUMN	Equal	0.87	8@190c/c
277	828	TENSION COLUMN	Equal	0.87	8@190c/c
278	1306.51	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c
279	2491.77	SHORT COLUMN	Equal	1.4	8@300c/c
280	4172.3	SHORT COLUMN	Equal	2.79	8@300c/c
281	1847.08	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
282	1440	TENSION COLUMN	Equal	0.89	8@255c/c
283	1795.69	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
284	2462.51	SHORT(Z) /BRACED LONG(Y)	Equal	1.82	8@230c/c
285	1440	TENSION COLUMN	Equal	0.89	8@255c/c
286	1934.32	SHORT(Z) /BRACED LONG(Y)	Equal	1.75	8@230c/c
287	1414.75	SHORT(Z) /BRACED LONG(Y)	Equal	1.17	8@230c/c
288	1440	TENSION COLUMN	Equal	0.89	8@255c/c
	1345.32	SHORT(Z) /BRACED LONG(Y)	Equal	0.98	8@190c/c

M. DATTA TRI P. A. C.
 STRUCTURAL ENGINEER,
 GHMC. Ls. No.: 134

BEAM DESIGN DETAILS

Memb No

18	Top Left Ast	Top Cen Ast	Top Rht Ast	Bot Left Ast	Bot Cen Ast	Bot Rht Ast	Stirrup Dia	Left Spacing	Cen Spacing	Right Spacing
19	747.99	105.18	852.63	314.61	299.68	431.4	2L 8	110	110	110
20	614.02	105.18	588.21	174.52	144.12	165.11	2L 8	110	110	110
21	524.1	105.57	478.85	415.11	105.18	342.61	2L 8	110	110	110
22	600.27	105.57	532.1	477.31	105.57	482.46	2L 8	110	110	110
23	325.27	105.18	290.33	176.78	105.18	192.76	2L 8	110	110	110
24	406.29	105.57	375.8	250.49	105.57	267.9	2L 8	110	110	110
25	418.43	105.57	403.81	273.31	105.57	283.83	2L 8	110	110	110
26	840.55	105.57	944.95	406.81	299.79	525.53	2L 8	110	110	110
27	526.93	105.57	528.02	182.97	110.49	181.56	2L 8	110	110	110
28	844.93	105.18	839.92	423.17	324.4	417.81	2L 8	110	110	110
29	768.58	105.57	761.25	344.26	265.33	336.41	2L 8	110	110	110
30	507.94	105.57	521.41	241.76	105.57	237.18	2L 8	110	110	110
31	268.44	105.57	232.49	199.18	105.57	260.83	2L 8	110	110	110
32	237.98	105.57	221.05	105.57	105.57	113.85	2L 8	110	110	110
33	231.46	105.57	258.97	146.49	105.57	130.44	2L 8	110	110	110
34	331.99	105.57	406.59	377.26	105.57	302.65	2L 8	110	110	110
35	392.57	105.57	278.17	189.89	105.57	248.99	2L 8	110	110	110
36	498.18	105.57	474.68	285.28	105.18	312.95	2L 8	110	110	110
37	1115.85	105.18	1123.44	733.75	501.76	742.03	2L 8	110	110	110
38	780.36	105.57	758.79	356.87	266.07	333.78	2L 8	110	110	110
39	511.09	105.57	517.88	239.2	105.57	238.64	2L 8	110	110	110
40	386.91	105.57	412.93	258.46	105.57	260.71	2L 8	110	110	110
41	399.73	105.57	401.95	264.72	105.57	262.33	2L 8	110	110	110
42	977.12	104.4	867.61	551.68	333.91	434.05	2L 8	110	110	110
60	321.24	105.57	314.88	265.14	105.57	233.83	2L 8	110	110	110
61	881.42	152.1	152.1	231.66	419.18	525.6	2L 8	140	140	140
62	920.07	152.1	763.88	332.07	177.28	288.8	2L 8	140	140	140
63	547.38	152.49	413.43	431.01	152.1	321.57	2L 8	140	140	140
64	728.82	152.49	656.14	762.99	164.67	445.83	2L 8	140	140	140
65	1082.1	152.1	152.1	448.16	452.92	586.79	2L 8	140	140	140
66	741.01	152.1	960.08	355.7	428.19	298.7	2L 8	140	140	140
67	761.88	152.49	937	344.89	374.42	299.12	2L 8	140	140	140
68	961.82	152.1	1299.88	403.12	400.26	673.47	2L 8	140	140	140
69	819.57	152.49	832.62	502.27	152.49	477.61	2L 8	140	140	140
70	1298.45	166.99	254.39	671.98	333.85	902.08	2L 8	140	100	140
71	1171.97	152.49	151.32	533.97	323.05	753.38	2L 8	140	140	140
73	776.89	152.1	817.83	519.34	152.1	543.22	2L 8	140	140	140
74	1536.59	151.32	802.82	918.66	399.92	1424.23	2L 8	140	135	140
75	1587.71	151.32	514.57	971.9	318.45	1155.31	2L 8	140	135	140


H. DATTATRI RAO
 STRUCTURAL ENGINEER
 No. 134

76	886.32	152.1	767.92	556	152.1	513.76	2L 8	140	140	14
77	357.41	152.49	605.26	273.71	152.49	179.98	2L 8	140	140	14
78	728.1	152.49	731.03	473.92	152.1	549.46	2L 8	140	140	14
79	1376.85	935.66	756.41	762.71	272.92	152.49	2L 8	120	125	12
80	1246.97	152.49	150.54	608.55	324.05	705.57	2L 8	140	135	14
81	820.45	152.49	852.79	509.96	152.49	538.43	2L 8	140	140	14
82	1280.73	151.32	946.73	652.87	388.94	393.96	2L 8	140	140	14
83	888.06	152.1	702.61	289.53	296.32	311.18	2L 8	140	140	14
84	908.12	152.1	782.82	289.91	323.67	327.43	2L 8	140	140	14
85	151.32	217.95	1160.11	784.13	306.67	521.53	2L 8	140	105	14
86	551.35	182.69	1594.32	1190.52	276.42	978.79	2L 8	140	105	14
87	170.2	152.49	745.08	404.44	549.35	151.32	2L 8	140	140	14
88	151.32	172.25	1163.81	710.86	309.36	525.41	2L 8	140	120	14
89	727.57	152.49	152.99	152.1	382.32	276.63	2L 8	140	140	14
90	227.85	152.65	1250.74	875.82	332.32	608.39	2L 8	140	110	14
91	810.47	151.32	1980	1431.55	271.72	1418.84	2L 8	140	120	14
92	187.15	152.49	781.16	427.78	598.08	150.54	2L 8	140	140	14
93	284.29	197.87	1658.49	945.24	209.75	1053.95	2L 8	140	105	14
94	786.54	151.32	152.49	152.49	449.97	326.99	2L 8	140	140	14
95	709.93	152.49	304.57	321.52	729.99	966.25	2L 8	140	140	14
96	848.89	152.49	308.51	294.48	227.72	152.49	2L 8	140	140	14
97	239.48	152.49	152.49	152.49	175.47	224.36	2L 8	140	140	14
98	864.66	518.59	354.73	223.38	167.8	152.49	2L10	135	135	13
99	195.09	514.24	1223.35	492.71	175.31	577.28	2L 8	140	90	14
100										
118	152.1	152.1	165.16	155.59	220.85	152.1	2L 8	140	140	14
119	886.54	152.1	152.1	236.96	405.96	525.43	2L 8	140	140	14
120	894.21	152.49	748.3	305.36	183.13	273.77	2L 8	140	140	14
121	432.87	152.49	361.41	354.04	152.49	265.29	2L 8	140	140	14
122	603.5	152.49	615.54	713.18	168.91	367.62	2L 8	140	140	14
123	1079.45	152.1	152.1	445.39	428.5	562.95	2L 8	140	140	14
124	751.53	152.1	944.6	331.86	411.85	282.66	2L 8	140	140	14
125	878.33	152.1	1118.37	376.26	487.5	486.94	2L 8	140	140	14
126	940.88	151.32	1214.45	388.07	401.08	568.02	2L 8	140	140	14
127	794.75	152.1	755.49	420.57	152.1	436.14	2L 8	140	140	14
128	1306.2	177.04	259.56	680.08	324.59	907.04	2L 8	140	100	14
129	1162.27	152.49	151.32	523.8	328.8	764.26	2L 8	140	135	14
130	683.96	152.49	791.51	494.08	152.49	449.77	2L 8	140	140	14
131	1632.64	151.32	777.17	1022.63	348.84	1402.32	2L 8	140	125	14
132	1572.65	151.32	514.96	956.22	319.82	1155.68	2L 8	140	135	14
133	786.87	152.1	773.03	551.72	152.1	459.99	2L 8	140	140	14
134	323.14	152.49	648.8	255.45	152.49	164.54	2L 8	140	140	14
135	709.35	152.49	597.67	379.36	152.49	508.87	2L 8	140	140	14
136	1410.87	930.57	737.66	801.7	267.66	152.49	2L 8	130	130	14
137	1222.14	152.49	151.32	588.88	322.74	702.66	2L 8	140	140	14

W. H. Adams, Jr.

138	698.49	152.49	834.79	478.96	152.49	418.44	2L 8	140	140	140
139	1207	152.1	915.2	564.6	386.13	375.79	2L 8	140	140	140
140	1055.16	152.1	819.29	418.6	411.98	346.61	2L 8	140	140	140
141	853.93	152.1	702.32	259.62	333.09	278.72	2L 8	140	140	140
142	151.32	208.92	1150.4	777.62	288.33	511.36	2L 8	140	110	140
143	543.31	183	1609.9	1184.65	266.61	998.94	2L 8	140	105	140
144	170.37	152.49	741.84	403.2	550.15	151.32	2L 8	140	140	140
145	151.32	168.47	1161.28	700.95	282.24	522.77	2L 8	140	125	140
146	719.9	152.49	152.49	152.1	388.47	281.74	2L 8	140	140	140
147	234.17	152.1	1229.96	881.87	335.8	586.69	2L 8	140	110	140
148	788.78	151.32	1923.71	1410.8	273.69	1359.01	2L 8	140	125	140
149	189.62	152.49	782.32	417.12	587.39	150.54	2L 8	140	140	140
150	286.68	187.81	1659.75	947.53	198.94	1055.25	2L 8	140	115	140
151	788.13	151.32	152.49	152.49	460.12	337.99	2L 8	140	140	140
152	670.11	152.1	297.64	325.54	728.59	959.05	2L 8	140	140	140
153	944.12	152.1	364.24	282.16	307.29	207.07	2L 8	140	140	140
154	218.65	152.1	152.1	152.1	170.08	183.22	2L 8	140	140	140
155										
156	173.03	475.65	1202.41	492.71	159.07	565.88	2L 8	140	95	140
157										
175	152.49	152.49	152.49	153.17	224.13	152.49	2L 8	140	140	140
176	845.42	152.1	152.1	194.38	408.44	533.51	2L 8	140	140	140
177	831.76	152.49	693.13	257.79	187.52	234.12	2L 8	140	140	140
178	298.8	152.49	278.12	240.2	152.49	177.55	2L 8	140	140	140
179	406.31	152.49	506.91	556.65	155.85	250.32	2L 8	140	140	140
180	980.72	151.32	151.32	321.19	405.93	564.22	2L 8	140	140	140
181	704.43	152.1	905.77	302.52	418.48	257.33	2L 8	140	140	140
182	820.16	152.1	1037.47	334.85	490	399.54	2L 8	140	140	140
183	860.79	152.1	1136.84	334.72	405.14	506.22	2L 8	140	140	140
184	718.79	152.49	631.79	297.2	152.1	334.35	2L 8	140	140	140
185	1246.48	164.24	263.79	603.94	295.85	910.22	2L 8	140	100	140
186	1123.96	152.49	152.1	492.78	304.94	763.73	2L 8	140	130	140
187	506.81	152.49	705.18	367.68	152.49	300.73	2L 8	140	140	140
188	1636.42	151.32	779.59	1026.57	324.58	1404.64	2L 8	140	130	140
189	1540.87	151.32	513.47	923.12	290.8	1154.25	2L 8	140	140	140
190	675.57	152.49	708.36	433.75	152.1	333.82	2L 8	140	140	140
191	279.29	152.49	545.62	191.76	152.1	152.1	2L 8	140	140	140
192	592.74	152.49	392.49	238.77	152.49	375.72	2L 8	140	140	140
193	1424.1	907.7	716.03	815.75	244	152.49	2L 8	140	140	140
194	1163.89	152.49	151.32	525.5	308.57	703.94	2L 8	140	140	140
195	521.95	152.49	768.1	371.42	152.49	279.94	2L 8	140	140	140
196	1126.29	152.1	848.4	495.2	392.56	326.21	2L 8	140	140	140
197	958.11	152.1	754.72	296.66	412.2	305.28	2L 8	140	140	140
198	796.17	152.1	644.12	221.32	334.56	254.49	2L 8	140	140	140
199	152.1	187.28	1121.01	780.61	264.43	489.69	2L 8	140	105	140

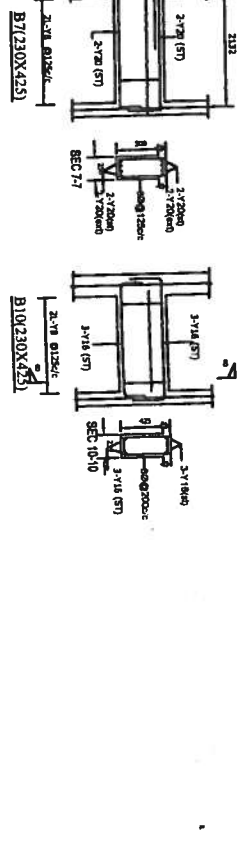
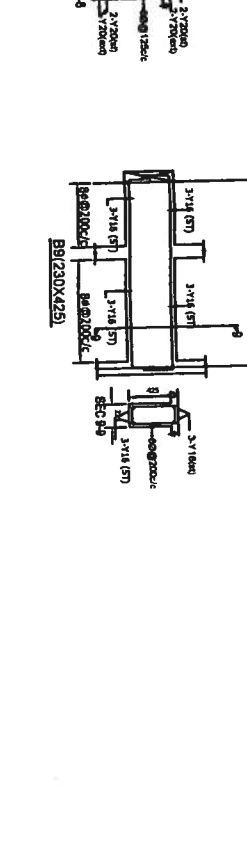
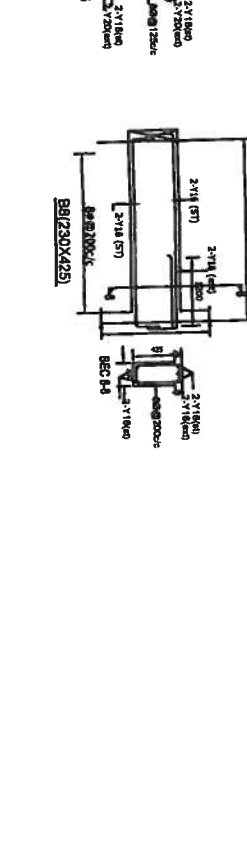
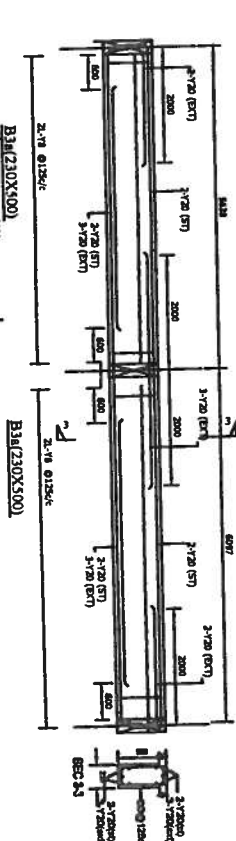
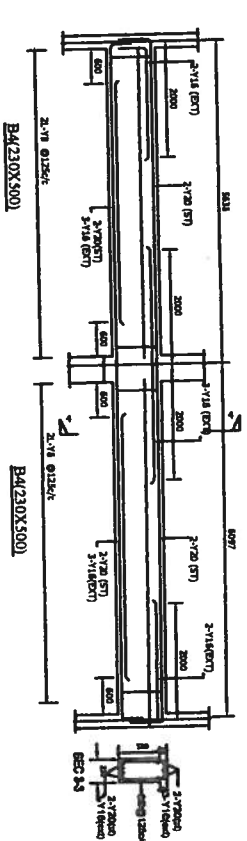
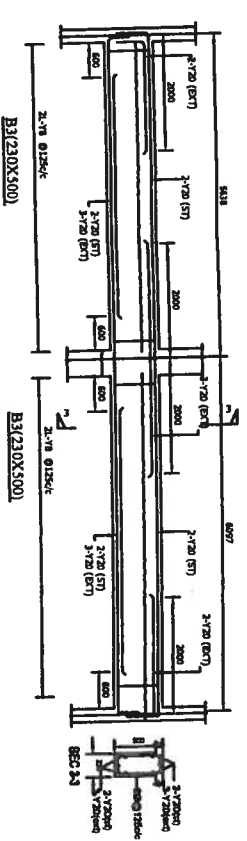
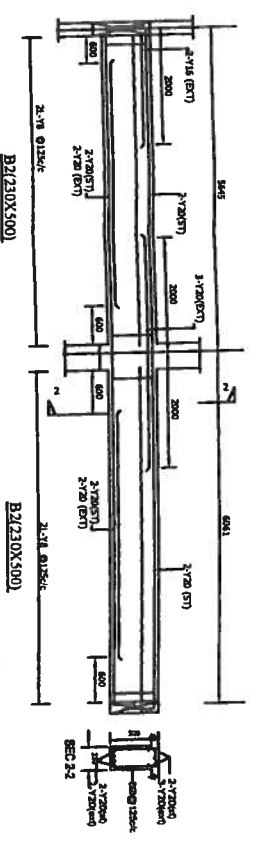
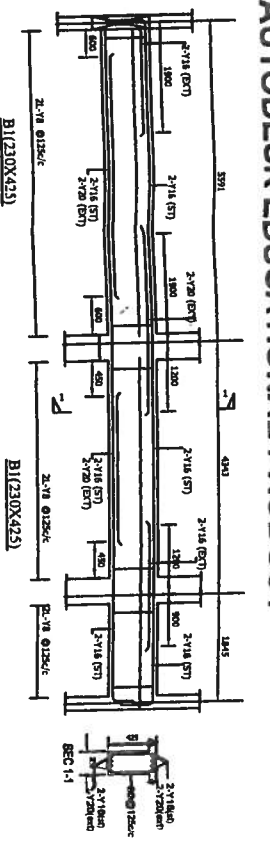
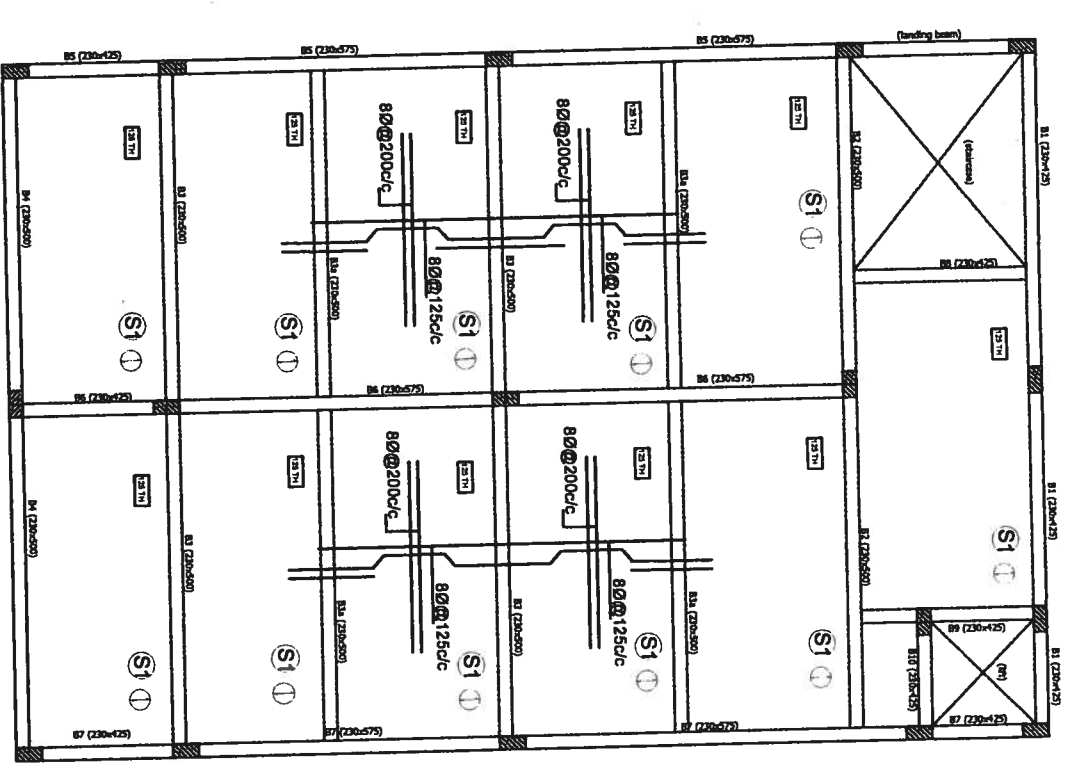
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 W. H. [Signature]
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200	546.3	155.69	1569.57	1185.69	240.71	953.01	2L 8	140	110	140
201	162.06	152.49	735.69	404.01	553.23	151.32	2L 8	140	140	140
202	152.1	153.36	1151.75	704.31	255.51	524.56	2L 8	140	125	140
203	711.59	152.49	152.49	152.1	388.82	280.02	2L 8	140	140	140
204	233.87	152.1	1179.58	882.37	315.57	536.17	2L 8	140	110	140
205	791.03	151.32	1889.29	1412.95	254.86	1309.23	2L 8	140	130	140
206	181.45	152.49	774.59	419.12	592.36	150.54	2L 8	140	140	140
207	292.07	169.4	1660.24	952.72	182.75	1055.76	2L 8	140	115	140
208	791.43	152.1	152.49	152.49	463.76	339.18	2L 8	140	140	140
209	647.56	152.1	299.35	308.07	728.52	960.71	2L 8	140	140	140
210	909.1	152.49	338.57	260.33	287.22	210.97	2L 8	140	140	140
211	214.96	152.1	152.1	152.1	170.64	177.7	2L 8	140	140	140
212	963.66	558.05	342.81	302.41	152.1	175.39	2L10	80	80	120
213	152.49	428.25	1146.64	469.59	152.49	507.42	2L 8	140	100	140
214	247.03	594.74	1321.33	584.01	213.47	695.9	2L10	140	85	140
232	152.49	152.49	152.49	152.1	222.59	152.1	2L 8	140	140	140
233	778.46	152.49	152.49	152.49	404.83	536.31	2L 8	140	140	140
234	730.96	152.49	565.15	182.36	189.53	188.76	2L 8	140	140	140
235	161.64	152.49	170.41	152.49	152.49	152.49	2L 8	140	140	140
236	206.68	152.49	349.53	351.48	152.49	152.49	2L 8	140	140	140
237	905.39	152.1	152.1	256.93	390.58	552.89	2L 8	140	140	140
238	622.28	152.1	793.49	237.27	410.62	166.41	2L 8	140	140	140
239	712.05	152.1	908.86	270.82	486.28	260.08	2L 8	140	140	140
240	728.68	152.1	964.76	278.94	402.26	303.55	2L 8	140	140	140
241	537.8	152.49	428.86	172.81	152.1	191.23	2L 8	140	140	140
242	1253.06	152.1	265.18	610.82	261.35	911.54	2L10	140	100	140
243	1044.04	152.49	152.1	406.34	272.5	771.13	2L 8	140	130	140
244	302.65	152.49	502.89	210.94	152.1	166.41	2L 8	140	140	140
245	1719.02	151.32	772.4	1127.78	262.05	1397.73	2L 8	140	135	140
246	1541.41	151.32	513	923.68	244.02	1153.81	2L 8	140	140	140
247	434.51	152.49	504.87	248.4	152.49	184.53	2L 8	140	140	140
248	191.83	152.49	440.99	152.49	152.49	152.49	2L 8	140	140	140
249	414.1	152.1	200.32	152.1	152.1	212.22	2L 8	140	140	140
250	1436.57	907.3	688.26	828.99	243.59	152.49	2L 8	140	140	140
251	1100.11	152.49	152.1	467.88	279.4	709.8	2L 8	140	140	140
252	328.66	152.49	589.05	222.97	152.49	175.29	2L 8	140	140	140
253	961.75	151.32	717.1	301.47	395.19	276.88	2L 8	140	140	140
254	855.92	152.1	645.41	205.61	414.54	247.21	2L 8	140	140	140
255	700.58	152.49	545.72	152.1	333.54	193.82	2L 8	140	140	140
256	152.1	160.7	1056.42	784.91	226.62	419.17	2L 8	140	100	140
257	545.01	151.32	1565.76	1184.45	191.17	949.04	2L 8	140	115	140
258	152.49	152.49	730.84	400.31	552.47	151.32	2L 8	140	140	140
259	152.1	152.49	1097.29	706.77	213.84	464.94	2L 8	140	120	140
260	705.1	152.49	152.49	152.1	389.71	278.38	2L 8	140	140	140
261	239.64	152.1	1143.83	887.92	285.92	499.09	2L 8	140	105	140


M. DATTA TRIPATHI
 STRUCTURAL ENGINEER

262	772.12	151.32	1848.16	1397.46	215.7	1263.65	2L 8	140	125	14
263	174.18	152.49	773.05	413.64	587.35	150.54	2L 8	140	140	14
264	297.61	151.32	1663.72	958.04	156.47	1059.39	2L 8	140	110	14
265	791.23	152.1	152.49	152.49	466.93	341.36	2L 8	140	140	14
266	594.96	151.32	299.32	277.22	726.07	959.69	2L 8	140	140	14
267	819.68	152.49	303.56	175.87	276.1	228.13	2L 8	140	140	14
268	209.78	152.1	152.1	152.1	160.26	162.24	2L 8	140	140	14
269	902.79	474.44	280.41	253.79	152.49	152.49	2L 8	95	100	9
270	152.1	349.47	1064.44	438.31	152.1	428.23	2L 8	140	110	14
271	175.05	481.4	1188.55	515.87	152.49	551.35	2L 8	140	95	14
289	152.49	152.49	152.49	152.49	226.01	152.49	2L 8	140	140	14
290	333.28	152.49	152.49	152.49	292.64	341.38	2L 8	140	140	14
291	397.61	152.49	286.19	152.49	152.49	152.49	2L 8	140	140	14
292	152.49	152.49	152.49	152.49	152.49	152.49	2L 8	140	140	14
293	152.49	152.49	153.28	152.49	152.49	152.49	2L 8	140	140	14
294	517.14	152.49	152.49	152.1	358.03	436.43	2L 8	140	140	14
295	326.11	151.32	791.46	297.16	491.06	152.49	2L 8	140	140	14
296	335.74	152.49	733.11	249.3	420.6	152.1	2L 8	140	140	14
297	295.73	152.49	546.29	170.57	271.58	152.49	2L 8	140	140	14
298	241.58	152.49	218.11	152.49	152.49	152.49	2L 8	140	140	14
299	934.69	152.49	151.32	271.92	214.49	782.6	2L 8	140	110	14
300	772.89	152.49	152.49	151.32	169.94	591.15	2L 8	140	140	14
301	152.96	152.49	248.81	152.49	152.49	152.49	2L 8	140	140	14
302	1251.35	151.32	736.04	606.4	340.56	1360.33	2L 8	140	140	14
303	1461.47	152.1	480.58	849	157.18	1111.59	2L 8	140	140	14
304	296.21	152.49	216.74	152.49	152.49	152.49	2L 8	140	140	14
305	152.49	152.49	373.61	152.49	152.49	152.49	2L 8	140	140	14
306	192.17	152.49	152.49	152.49	152.49	152.49	2L 8	140	140	14
307	963.78	649.83	454.6	302.53	152.1	152.1	2L 8	140	140	14
308	858.57	152.49	152.49	208	169.56	528.62	2L 8	140	140	14
309	169.89	152.49	295.13	152.49	152.49	152.49	2L 8	140	140	14
310	517.22	152.49	280.03	152.49	237.66	152.49	2L 8	140	140	14
311	637.68	152.1	271.64	152.1	323.24	180.33	2L 8	140	140	14
312	706.85	152.49	275.86	152.49	364.42	204.5	2L 8	140	140	14
313	152.49	152.49	763.37	650.12	189.79	152.1	2L 8	140	135	14
314	507.48	152.1	1313.99	1139.06	163.58	688.23	2L 8	140	140	14
315	152.49	152.49	724.16	425.55	573.42	151.32	2L 8	140	140	14
316	152.49	152.49	795.69	547.78	188.25	152.1	2L 8	140	140	14
317	705.82	152.49	152.49	152.1	398.81	291.33	2L 8	140	140	14
318	152.1	152.49	860.95	735.59	200.49	210.46	2L 8	140	140	14
319	740.09	151.32	1732.95	1366.7	151.32	1142.43	2L 8	140	130	14
320	161.64	152.49	737.32	441.59	635.51	178.84	2L 8	140	140	14
321	150.54	152.49	1218.07	797.39	152.49	578.15	2L 8	140	140	14
322	743.69	152.49	152.49	152.49	469.66	332.23	2L 8	140	140	14
323	442.24	152.1	183.97	229.93	597.44	835.07	2L 8	140	140	14


M. DATTATRAYA
 STRUCTURAL ENGINEER
 192



- GENERAL NOTES**
1. USE M25 GRADE OF CONCRETE FOR COLUMNS, FOOTINGS, BEAMS & SLABS. (RATIO AS PER DESIGN MIX).
 2. USE FE 500 GRADE TOR STEEL.
 3. USE FE 500 GRADE TOR STEEL.
 4. FOOTING IS DESIGN FOR SHTLT & UPPER FOUR FLOORS.
 5. S.B.C OF THE SOIL IS TAKEN AS PER SOIL REPORT.
 6. USE FE 500 GRADE TOR STEEL.
 7. PROVIDE CLEAR COVER TO STEEL, 40mm FOR COLUMNS, 50mm FOR FOOTINGS, 25mm FOR BEAMS AND 20mm FOR SLABS.
 8. PROVIDE 25MM CAMBER AT FREE END FOR CANTILEVER BEAMS & SLABS.
 9. IN SLAB EXTEND VE STEEL UP TO 0.50L FROM FACE OF SUPPORT.
 10. DO NOT PROVIDE EXTRA REINFORCEMENT AT SQUARE SUPPORTS.
 11. LAP LENGTH 48 D (D IS THE DIA OF THE BAR) IN COMPRESSION.
 12. LAP LENGTH 52 D (D IS THE DIA OF THE BAR) IN TENSION.
 13. DESIGNED FOR ZONE-II EARTHQUAKE LOADS AS PER IS 1893 -2002 & WIND LOADS AS PER IS 875 PART-3.
 14. ALL THE DIMENSIONS ARE IN MILLIMETERS.

PLAN SHOWING THE PROPOSED GATED COMMUNITY LAYOUT CUM GROUPHOUSING IN SY. NO.789 (P) SITUATED AT MIRYALAGUDA VILLAGE AND MANDAL, NALGONDA DISTRICT, TELANGANA.

BELONGING TO:

1. MRS. A VASUDHA REDDY
W/O LATE SRI. VEERA REDDY
2. SRI. A. SUAY REDDY
S/O LATE SRI. VEERA REDDY
3. SRI. A. AJAY REDDY
S/O LATE SRI. VEERA REDDY

AMENITIES BLOCK

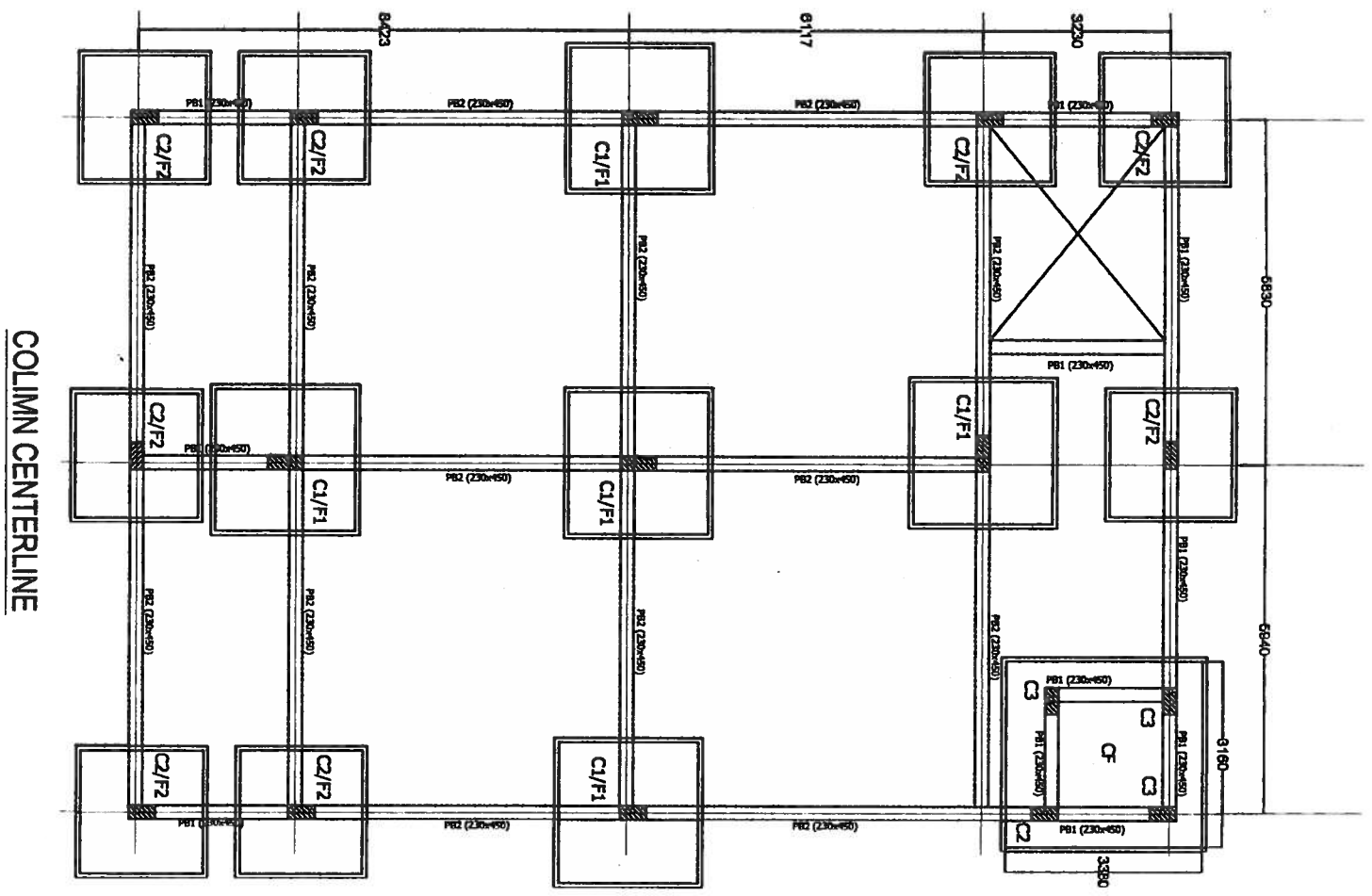
TYPICAL SLAB & BEAM SECTION DETAILS

Structural Engineer's Signature

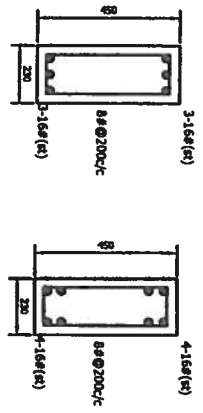
M. Dattatreya Rao

M. Dattatreya Rao
GHMC LICENSING ENGINEER
STRUCTURAL ENGINEER
GHMC. L. No.: 134

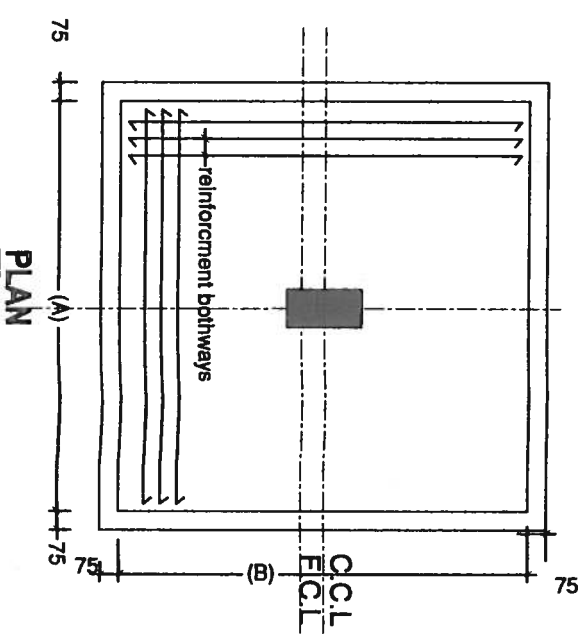




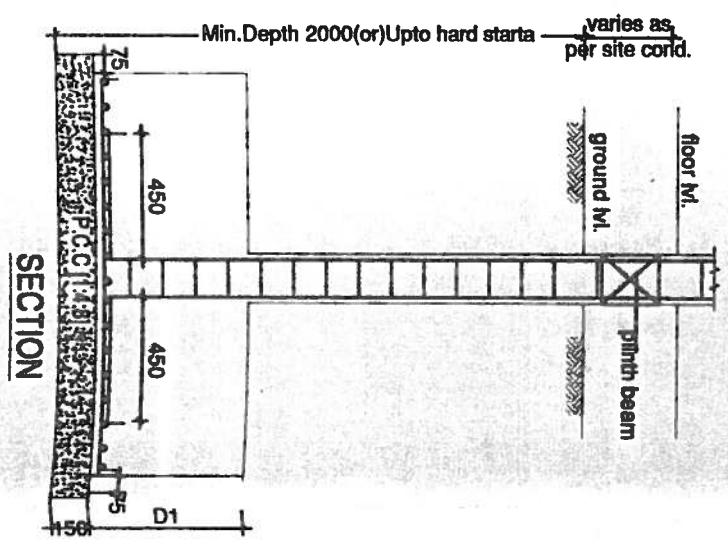
COLUMN SECTION DETAILS				FOOTING DETAILS						
TYPE	MIX	COLUMN SIZE	SECTION	REINFORCEMENT	SNO	FOOT SIZE	A	B	D1	REINFOR CEMENT
C1	M25	230x600		#4nos-25Ø +6-20Ø 8Ø@200 c/c 2-ties	1	F 1	2400	2400	750	16Ø@150c/c bothways
C2	M25	230x600		#8nos-20Ø +4-16Ø 8Ø@200 c/c 2-ties	2	F 2	2100	2100	600	12Ø@125c/c bothways
C3	M25	230x450		#4nos-20Ø +4-16Ø 8Ø@200 c/c 2-ties	3	F 3	1800	1800	525	12Ø@150c/c bothways
					4	CF	3160	3380	750	16Ø@150c/c bothways top & bottom



PLINTH BEAM SECTION



PLAN



SECTION

- GENERAL NOTES**
- USE M25 GRADE OF CONCRETE FOR COLUMNS, FOOTINGS, BEAMS & SLABS. (RATIO AS PER DESIGN MIX).
 - USE FE 500 GRADE FOR STEEL.
 - USE FE 500 GRADE FOR STEEL.
 - FOOTING IS DESIGN FOR STILL & UPPER FOUR FLOORS.
 - B.S.C OF the soil is taken as per soil report.
 - USE FE 500 GRADE FOR STEEL.
 - PROVIDE CLEAR COVER TO STEEL. Allow for columns, 50mm FOR FOOTING, 25mm SLAB AND 20mm FOR BEAMS.
 - PROVIDE 25MM CHAMFER AT FREE END FOR CANTILEVER BEAMS & SLABS.
 - IN SLAB EXTEND -1/2 STEEL UP TO 0.30L FROM FACE OF SUPPORT.
 - DO NOT PROVIDE EXTRA REINFORCEMENT AT SIMPLE SUPPORT.
 - LAP LENGTH 48 D (D - IS THE DIA OF THE BAR) IN COMPRESSIVE.
 - LAP LENGTH 52 D (D - IS THE DIA OF THE BAR) IN TENSION.
 - DESIGNED FOR ZONE-II EARTHQUAKE LOADS AS PER IS 1893 -2002 & WIND LOADS AS PER IS 875 PART-3.
 - ALL THE DIMENSIONS ARE IN MILLIMETERS.

PLAN SHOWING THE PROPOSED GATED COMMUNITY LAYOUT CUM GROUPHOUSING IN SY. NO.788 (P) SITUATED AT MIRIVALAGUDA VILLAGE AND MANDAL, NALGONDA DISTRICT, TELANGANA. BELONGING TO:

- MRS. AVASUDHA REDDY W/O.LATE SRI. VEERA REDDY
- SRI. A. SUJAY REDDY S/O.LATE SRI. VEERA REDDY
- SRI. A. AJAY REDDY S/O.LATE SRI. VEERA REDDY

AMBENTIES BLOCK

COLUMN & FOOTING SECTION DETAILS



Structural Engineer's Signature

M. Dattatreya
G.H.M.C License No. 134
M. DATTATREYA
STRUCTURAL ENGINEER
G.H.M.C. L.S. No. 134